

دارات الكترونية المحاضرة /5/ - عملي

الدكتور السموع صالحي
المهندس جبران خليل
المهندسة ايه خيربك

Depletion-type MOSFET

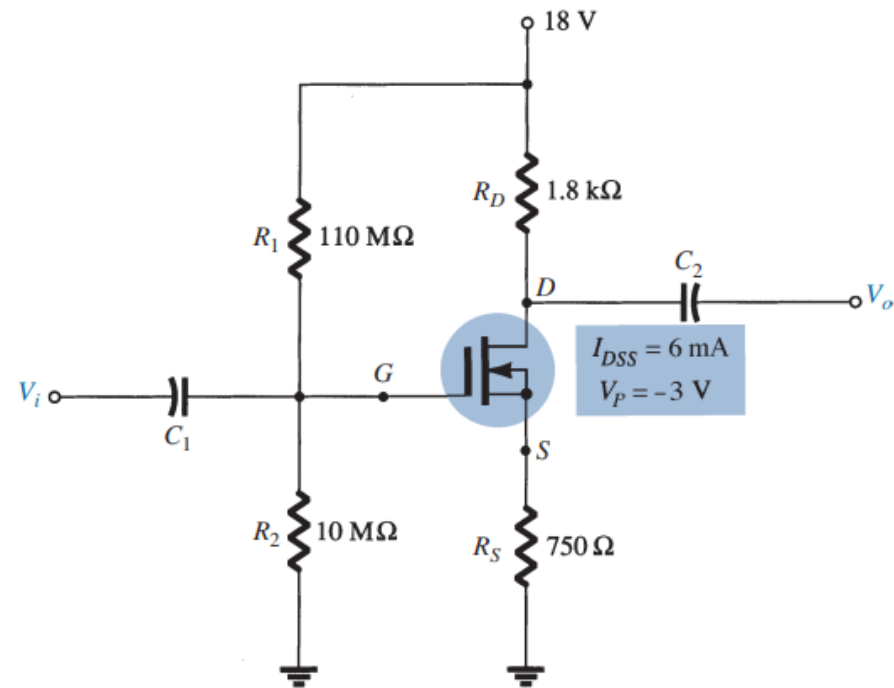
- The similarities in appearance between the transfer curves of **JFETs** and **depletion-type MOSFETs** permit a similar analysis of each in the dc domain.
- The primary difference between the two is the fact that depletion-type MOSFETs permit operating points with positive values of V_{GS} and levels of I_D that exceed I_{DSS} . In fact, for all the configurations discussed thus far, the analysis is the same if the JFET is replaced by a depletion-type MOSFET.

Depletion-type MOSFET

- For the n-channel depletion-type MOSFET of the following Fig, determine:

a. I_{DQ} and V_{GSQ} .

b. V_{DS} .



Depletion-type MOSFET

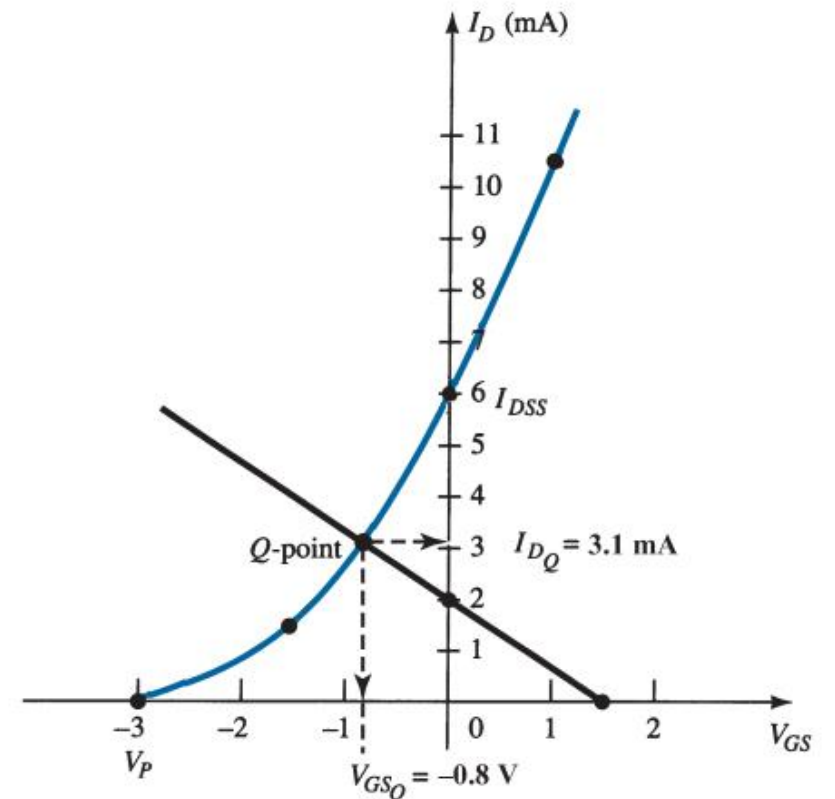
- For the transfer characteristics, a plot point is defined by $I_D = I_{DSS}/4 = 6 \text{ mA}/4 = 1.5 \text{ mA}$ and $V_{GS} = V_P/2 = -3 \text{ V}/2 = -1.5 \text{ V}$.
- Considering the level of V_P and the fact that Shockley's equation defines a curve that rises more rapidly as V_{GS} becomes more positive, a plot point will be defined at **$V_{GS} = +1 \text{ V}$** .
- Substituting into Shockley's equation yield

$$I_D = I_{DSS} \left(1 - \frac{V_{GS}}{V_p}\right)^2$$

Depletion-type MOSFET

$$I_D = I_{DSS} \left(1 - \frac{V_{GS}}{V_p}\right)^2$$

- $I_D = 6\text{mA} \left(1 - \frac{1}{-3}\right)^2$
- $I_D = 10.67\text{mA}$
- The resulting transfer curve appears in the Fig. behind Proceeding as described for JFETs, we have:



Depletion-type MOSFET

- From $V_G = \frac{R_2 V_{DD}}{R_1 + R_2} \Rightarrow V_G = \frac{10M\Omega(18V)}{10M\Omega + 110M\Omega} = 1.5v$
- $V_{GS} = V_G - I_D R_S = 1.5 - I_D (750\Omega)$
- Setting $I_D = 0$ mA results in FET Biasing

$$V_{GS} = V_G = 1.5 \text{ V}$$

- Setting $V_{GS} = 0$ V yields

$$I_D = \frac{V_G}{R_S} = \frac{1.5 \text{ v}}{750\Omega} = 2 \text{ mA}$$

Depletion-type MOSFET

- The plot points and resulting bias line appear in the previous Fig. The resulting operating point is given by

$$I_{DQ} = 3.1 \text{ mA}$$

$$V_{GSQ} = -0.8 \text{ v}$$

b. From $V_{DS} = V_{DD} - I_D (R_S + R_D) = 18 \text{ v} - (3.1 \text{ mA})(1.8 \text{ k}\Omega + 750 \Omega) = 10.1 \text{ v}$

الطريقة الحسابية لاجاد I_D

- $V_{GS} = V_G - I_D R_S = 1.5 \text{ v} - I_D (0.75 \text{ (K}\Omega))$

- $I_D = I_{DSS} \left(1 - \frac{V_{GS}}{V_p}\right)^2$

- $I_D = 6 \left(1 - \frac{1.5 - 0.75 I_D}{-3}\right)^2$

- $I_D = 6 (1.5 - 0.25 I_D)^2$

- $I_D = 6(2.25 - 0.75 I_D + 0.0625 I_D^2)$

- $I_D = (13.5 - 4.5 I_D + 0.375 I_D^2)$

- $0 = 13.5 - 5.5 I_D + 0.375 I_D^2$

- $\Rightarrow I_{D1} = 3.1 \text{ mA} \Rightarrow V_{GS} = -0.8 \text{ v}$

- $\Rightarrow I_{D2} = 11.5 \text{ mA} \Rightarrow V_{GS} = -7 \text{ v}$

الحل الثاني يعد مرفوض لان

$$V_{GS} > V_p$$

و بالتالي

$$I_D = 3.1 \text{ mA}$$