

# Lecture 10



## (BJT MODELING)

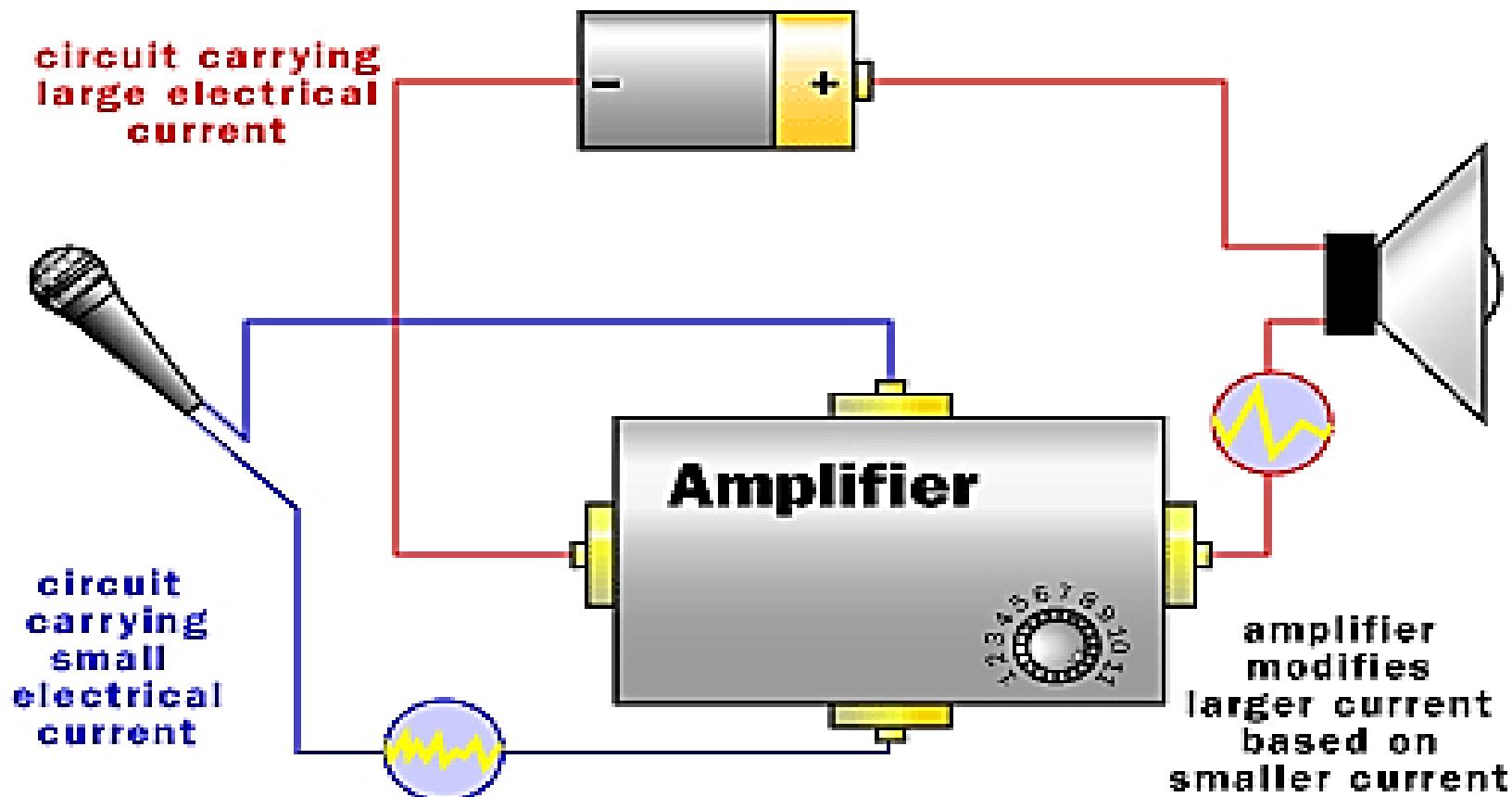
## الادارات المكافحة

DR. BASSAM ATIEH

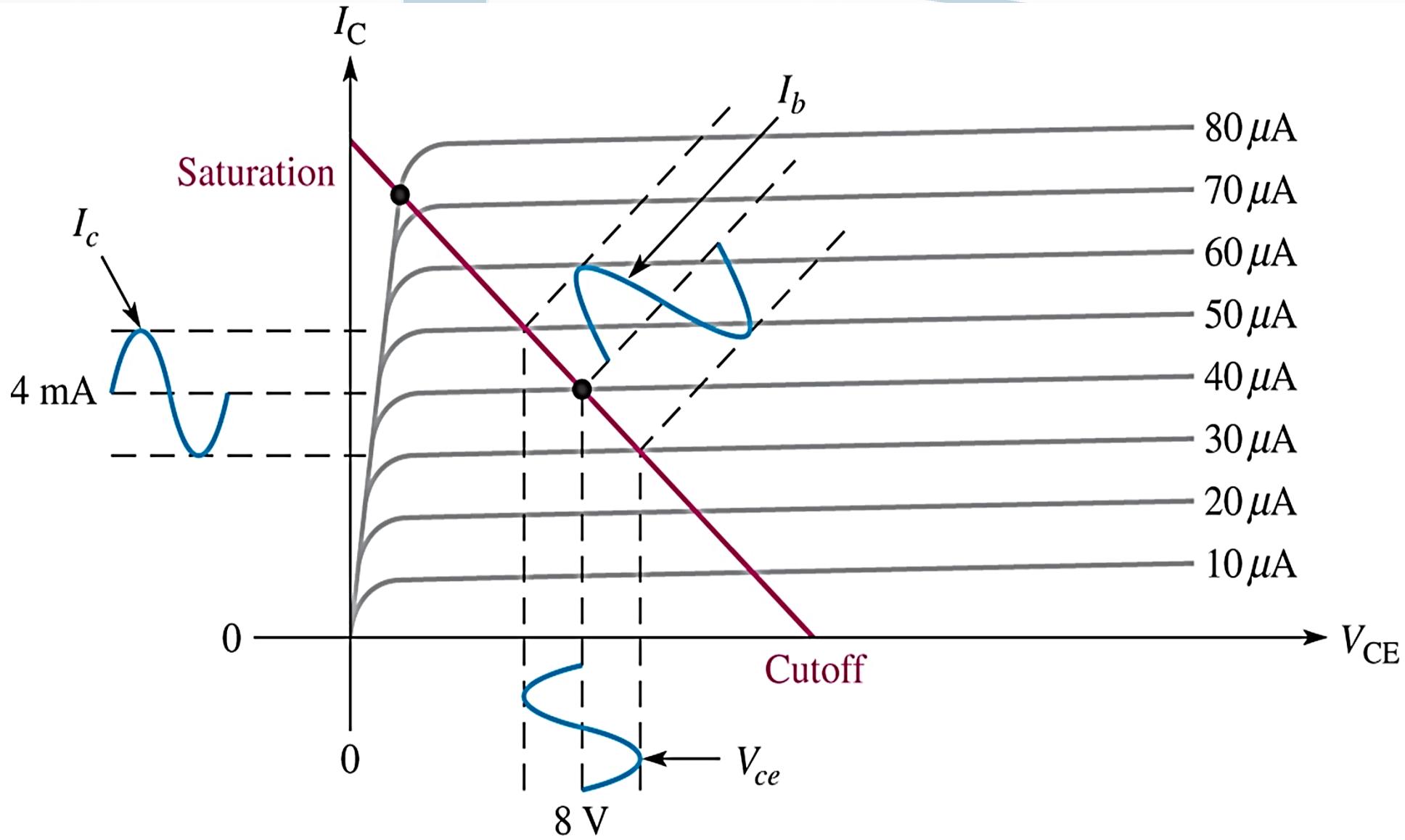
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## How Amplifiers Work



# Small-Signal Amplifier Operation



# BJT Transistor Modeling



- A model equivalent circuit that represents the AC characteristics of the transistor.
- A model uses circuit elements that approximate the behavior of the transistor.
- There are two models commonly used in small signal AC analysis of a transistor:
  - $r_e$  model
  - Hybrid equivalent model

## The $r_e$ Transistor Model

- BJTs are basically **current-controlled** devices; therefore the  $r_e$  model uses a diode and a current source to duplicate the behavior of the transistor.
- One **disadvantage to this model is its sensitivity to the DC level.**
- This model is designed for specific circuit conditions.

# Common-Base Configuration

$$I_c = \alpha I_e$$

$$r_e = \frac{26 \text{ mV}}{I_e}$$

**Input impedance:**

$$Z_i = r_e$$

**Output impedance:**

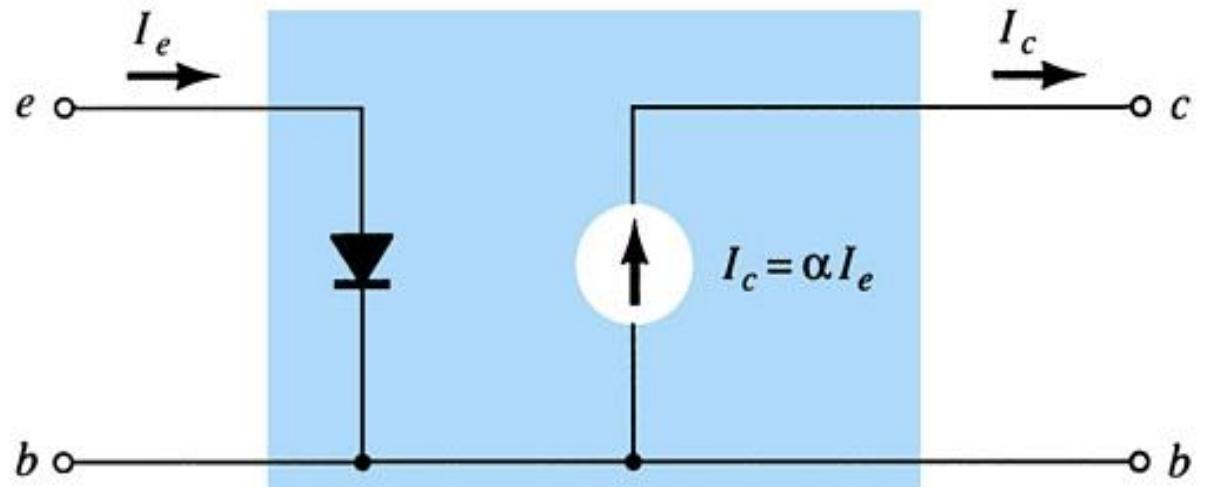
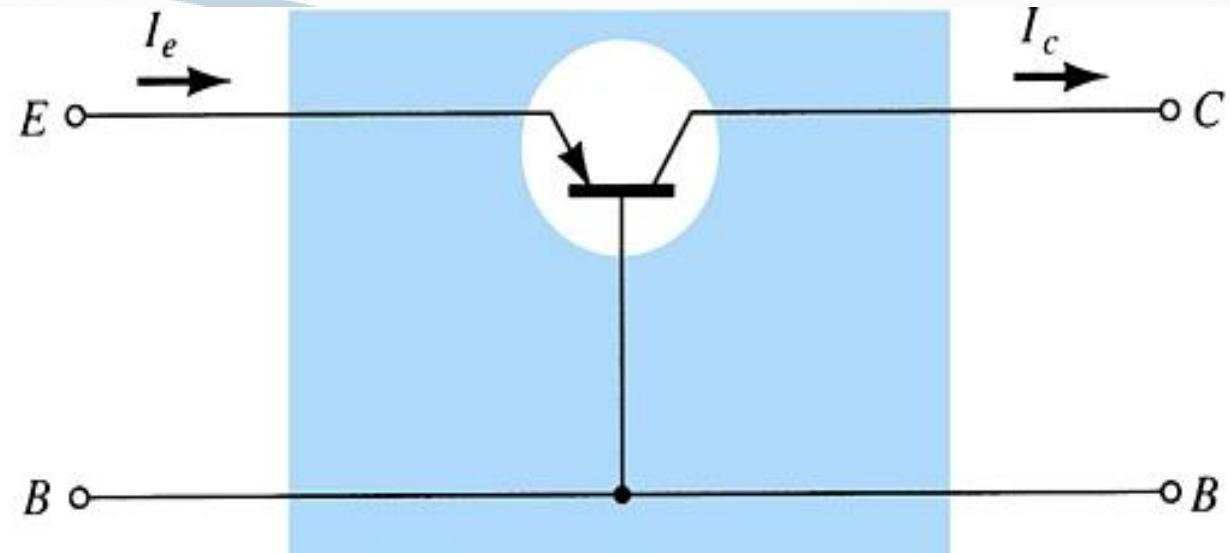
$$Z_o \cong \infty \Omega$$

**Voltage gain:**

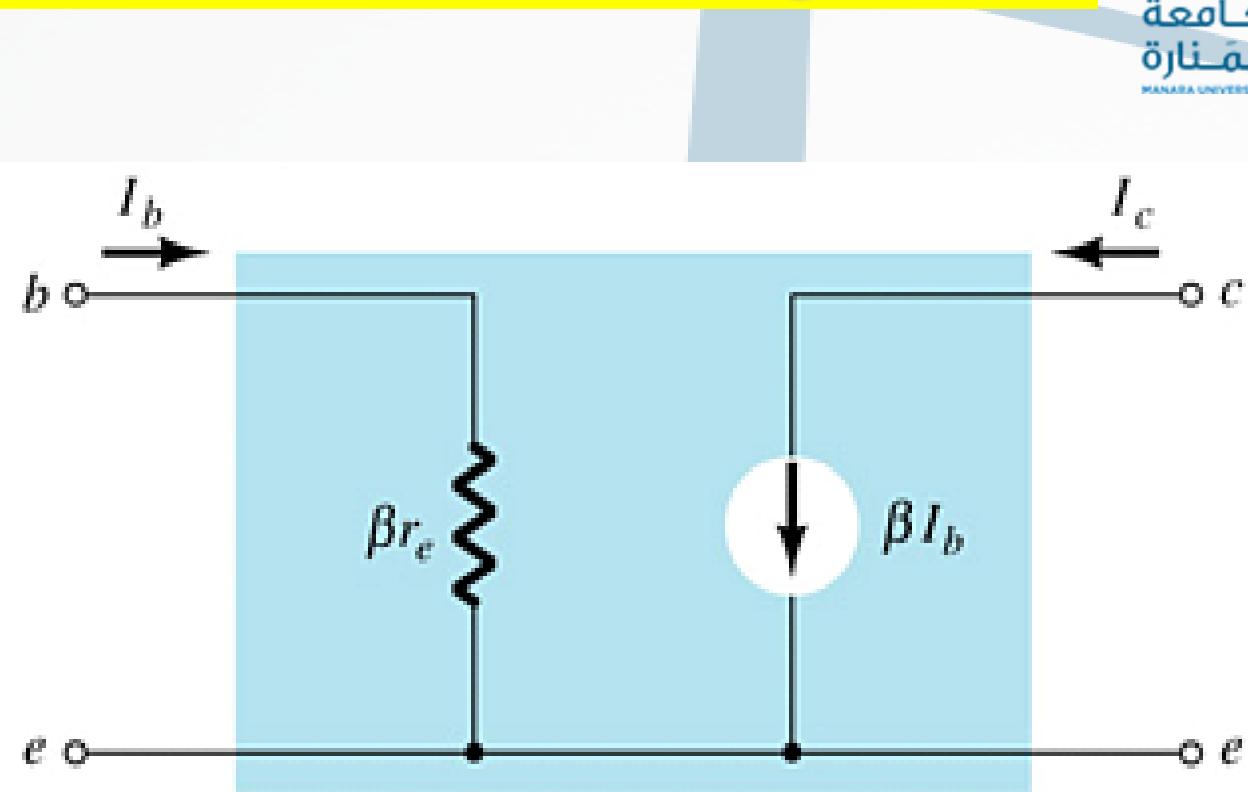
$$A_v = \frac{\alpha R_L}{r_e} \cong \frac{R_L}{r_e}$$

**Current gain:**

$$A_i = -\alpha \cong -1$$



## Common-Emitter Configuration



$$r_e = \frac{26 \text{ mV}}{I_e}$$

$$I_e = (\beta + 1)I_b \cong \beta I_b$$

**Input impedance:**

$$Z_i = \beta r_e$$

**Output impedance:**

$$Z_o = r_o \cong \infty \Omega$$

**Voltage gain:**

$$A_v = -\frac{R_L}{r_e}$$

**Current gain:**

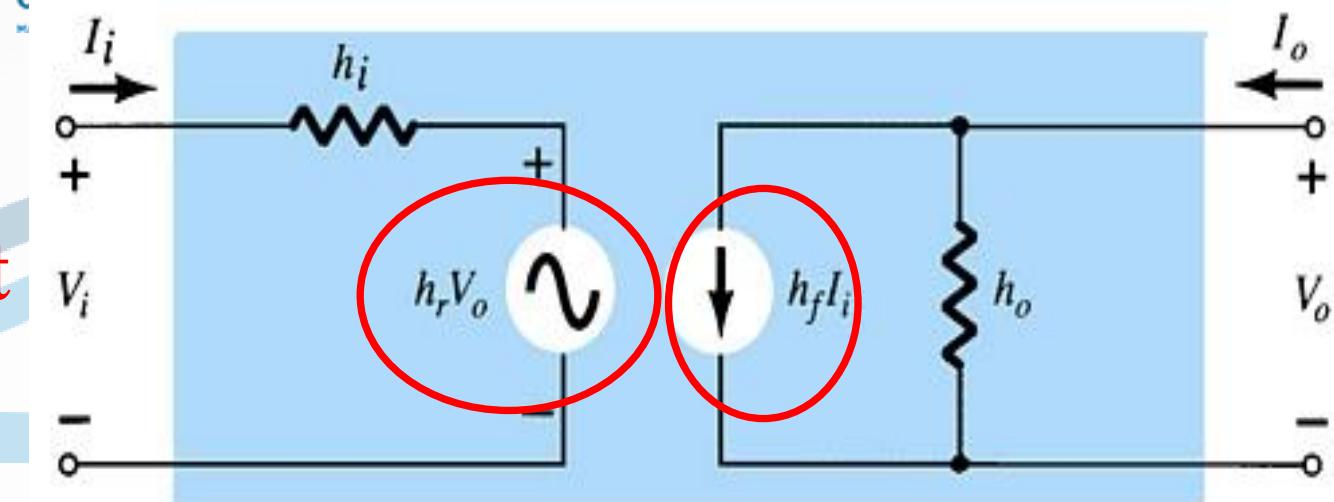
$$A_i = \beta \Big|_{r_o=\infty}$$

The diode  $r_e$  model can be replaced by the resistor  $r_e$ .

# The Hybrid Equivalent Model

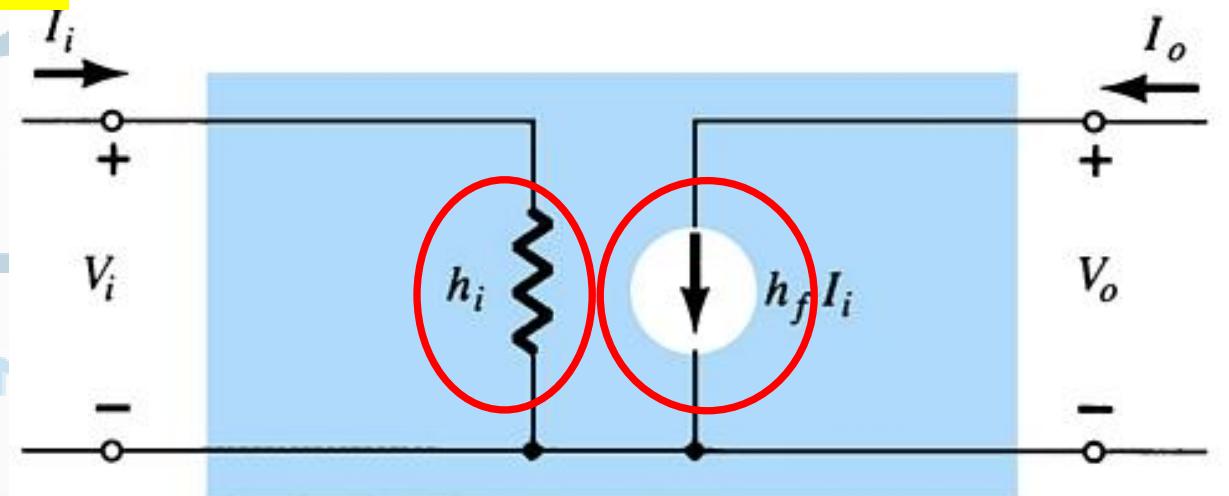


- $h_i$  = input resistance
- $h_r$  = reverse transfer voltage ratio ( $V_i/V_o \approx 0$ )
- $h_f$  = forward transfer current ratio ( $I_o/I_i$ )
- $h_o$  = output conductance



## Simplified General h-Parameter Model

- $h_i$  = input resistance
- $h_f$  = forward transfer current ratio ( $I_o/I_i$ )



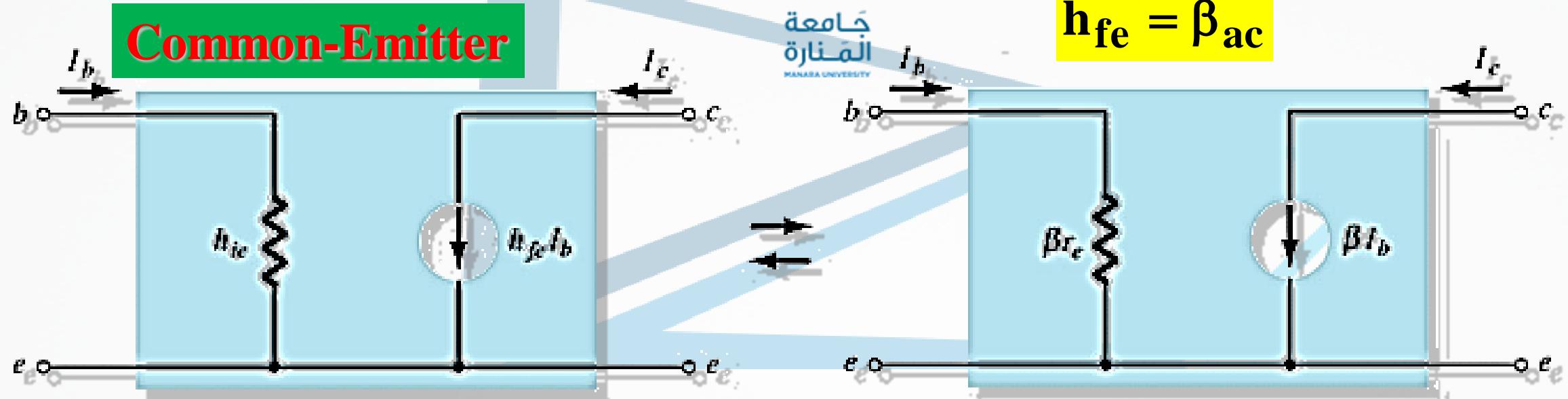
# re vs. h-Parameter Model



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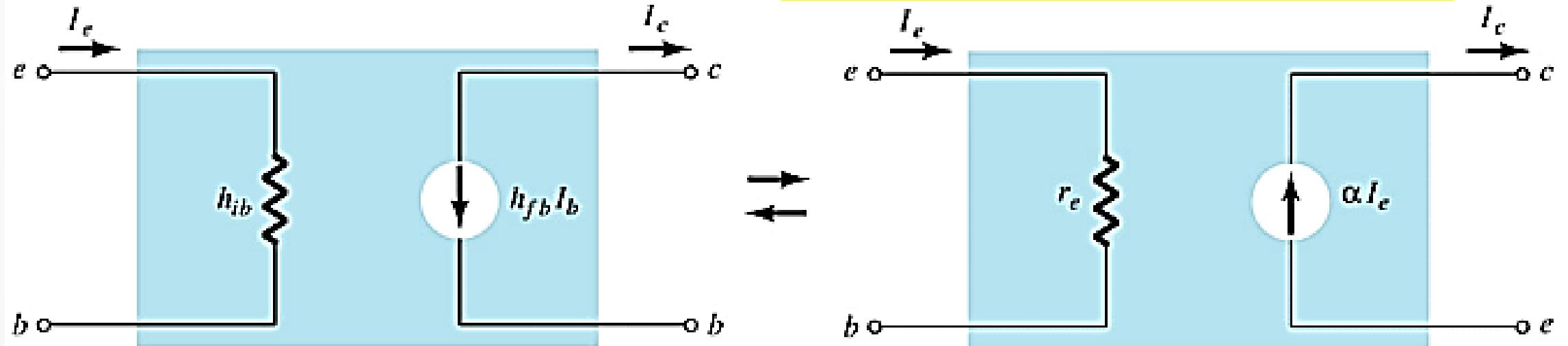
$$h_{ie} = \beta r_e$$

$$h_{fe} = \beta ac$$



# Common-Base

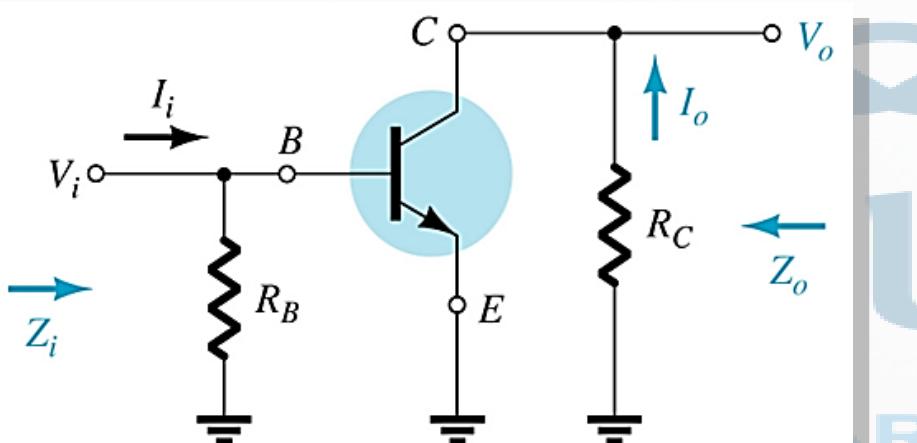
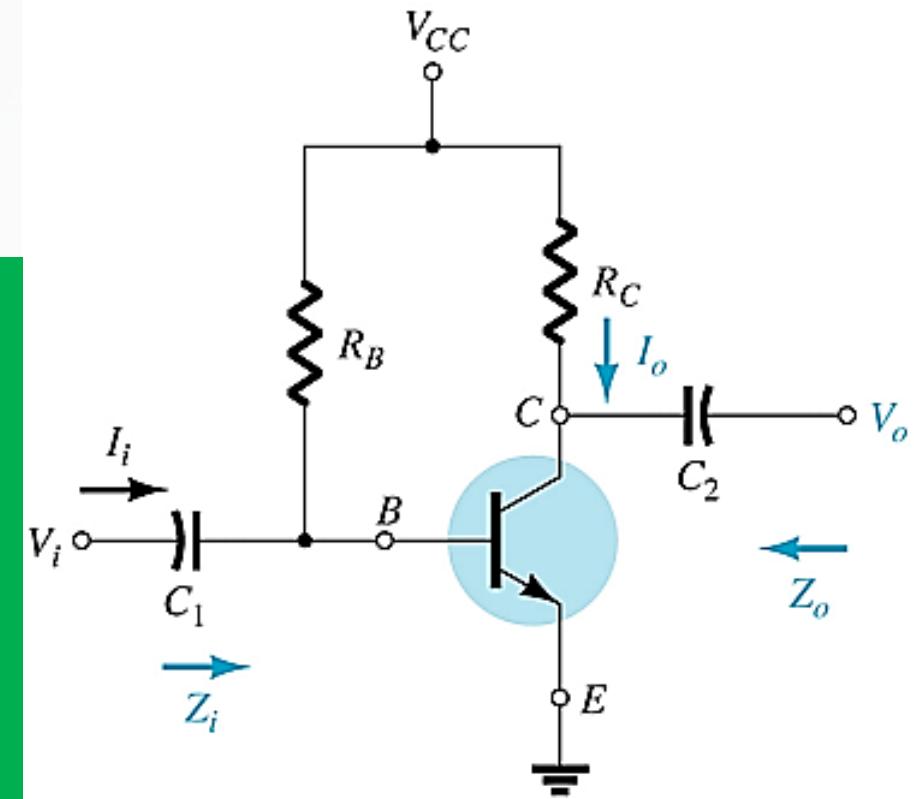
$$h_{ib} = r_e \quad ; \quad h_{fb} = -\alpha \approx -1$$



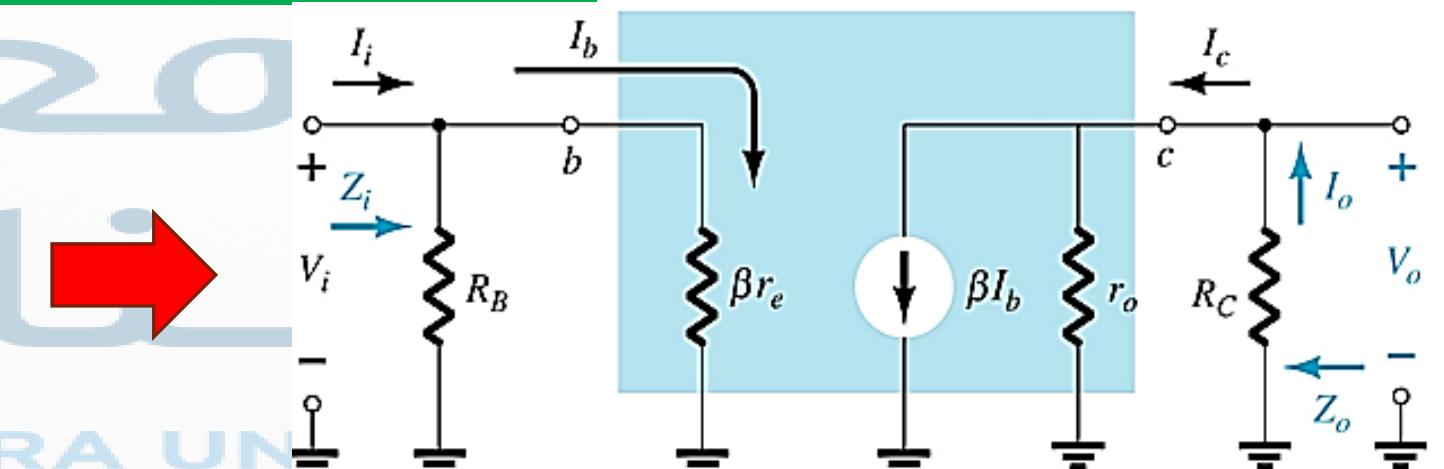
# Common-Emitter Fixed-Bias Configuration



- The input is applied to the base
- The output is from the collector
- High input impedance
- Low output impedance
- High voltage and current gain
- Phase shift between input and output is  $180^\circ$

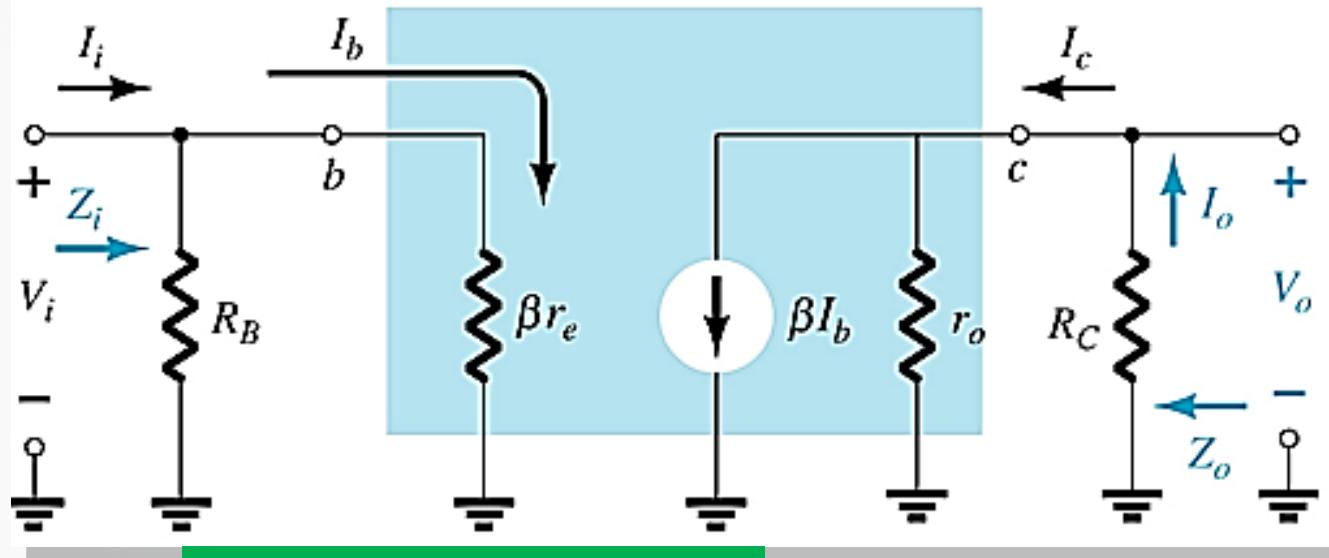


AC equivalent



re model

# Common-Emitter Fixed-Bias Calculations



Voltage gain:

$$A_v = \frac{V_o}{V_i} = -\frac{(R_C \parallel r_o)}{r_e}$$

$$A_v = -\frac{R_C}{r_e} \quad | \quad r_o \geq 10R_C$$

Current gain from voltage gain:

Input impedance:

$$Z_i = R_B \parallel \beta r_e$$

$$Z_i \approx \beta r_e \quad | \quad R_B \geq 10\beta r_e$$

Output impedance:

$$Z_o = R_C \parallel r_o$$

$$Z_o \approx R_C \quad | \quad r_o \geq 10R_C$$

$$A_i = \frac{I_o}{I_i} = \frac{\beta R_B r_o}{(r_o + R_C)(R_B + \beta r_e)}$$

Current gain:

$$A_i \approx \beta \quad | \quad r_o \geq 10R_C, R_B \geq 10\beta r_e$$

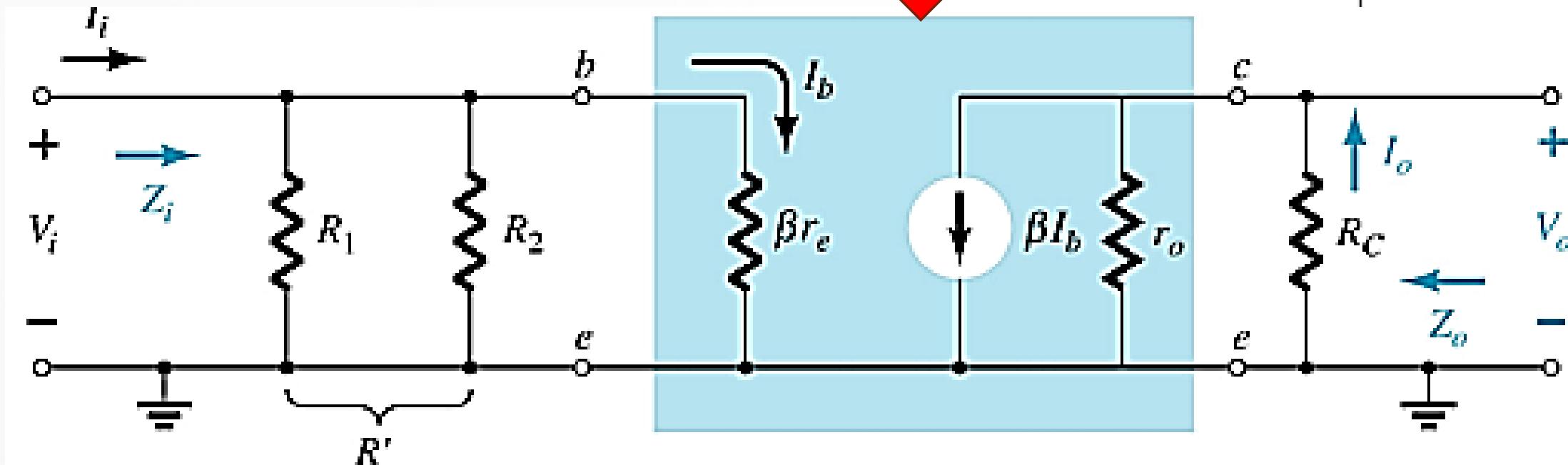
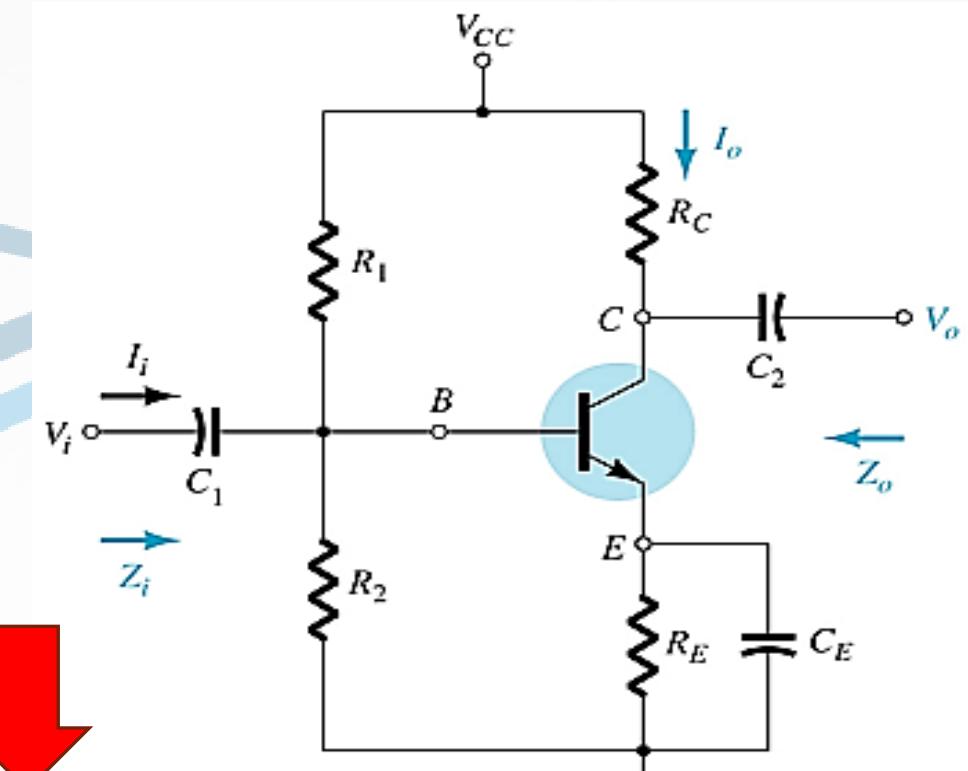
$$A_i = -A_v \frac{Z_i}{R_C}$$

# Common-Emitter Voltage-Divider Bias

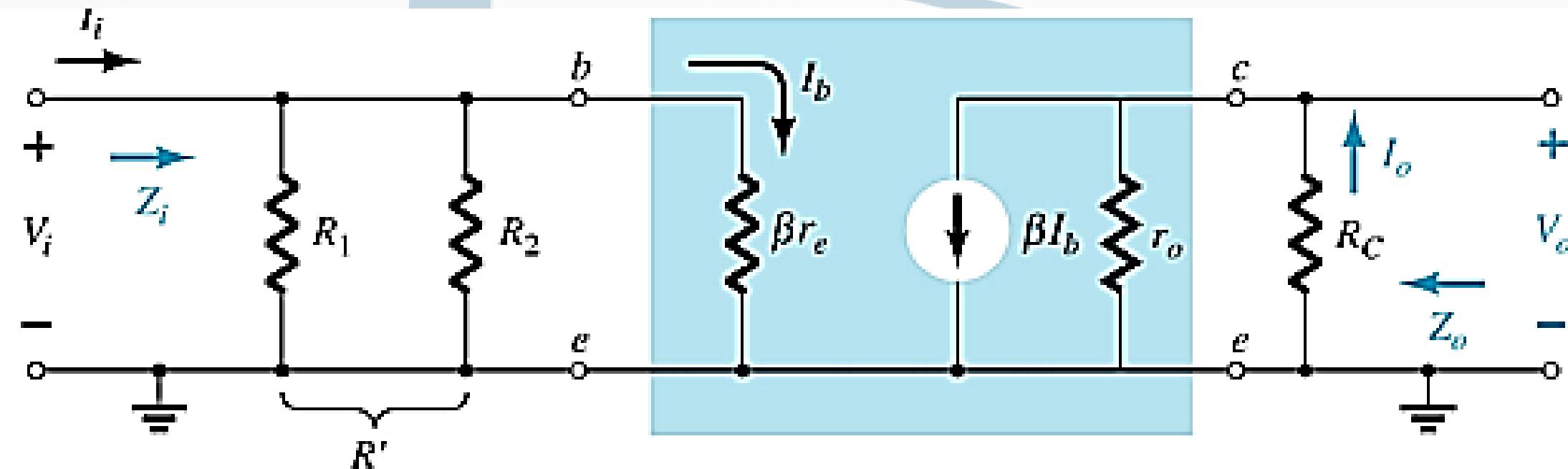


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$r_e$  model requires you to determine  $\beta$ ,  $r_e$ , and  $r_o$ .



# Common-Emitter Voltage-Divider Bias Calculations



**Input impedance:**

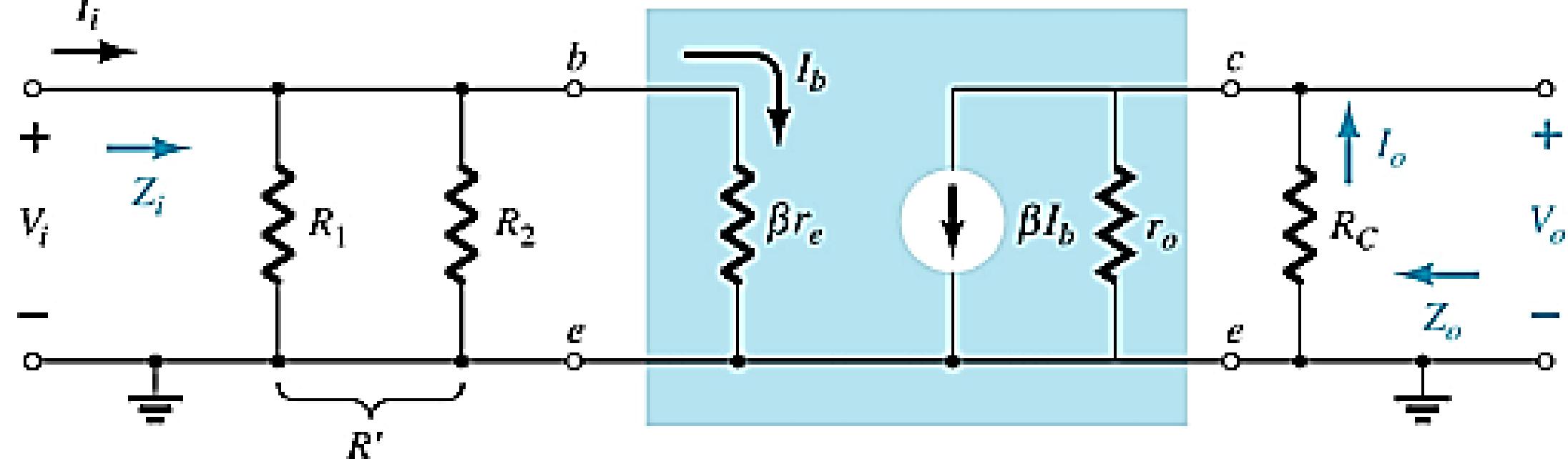
$$R' = R_1 \parallel R_2$$

$$Z_i = R' \parallel \beta r_e$$

**Output impedance:**

$$Z_o = R_C \parallel r_o$$

$$Z_o \approx R_C \quad | \quad r_o \geq 10R_C$$



**Voltage gain:**

$$A_v = \frac{V_o}{V_i} = \frac{-R_C \parallel r_o}{r_e}$$

$$A_v = \frac{V_o}{V_i} \approx -\frac{R_C}{r_e} \Big| r_o \geq 10R_C$$

**Current gain from voltage gain:**

$$A_i = -A_v \frac{Z_i}{R_C}$$

**Current gain:**

$$A_i = \frac{I_o}{I_i} = \frac{\beta R' r_o}{(r_o + R_C)(R' + \beta r_e)}$$

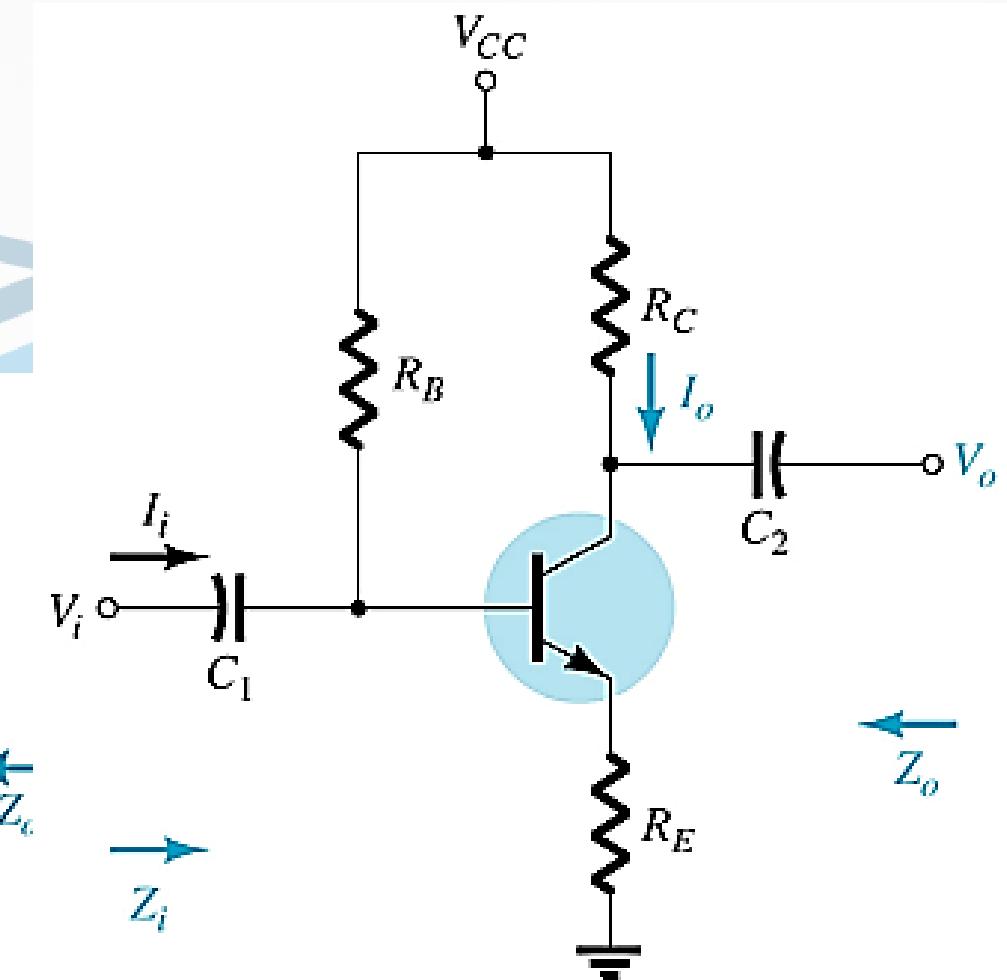
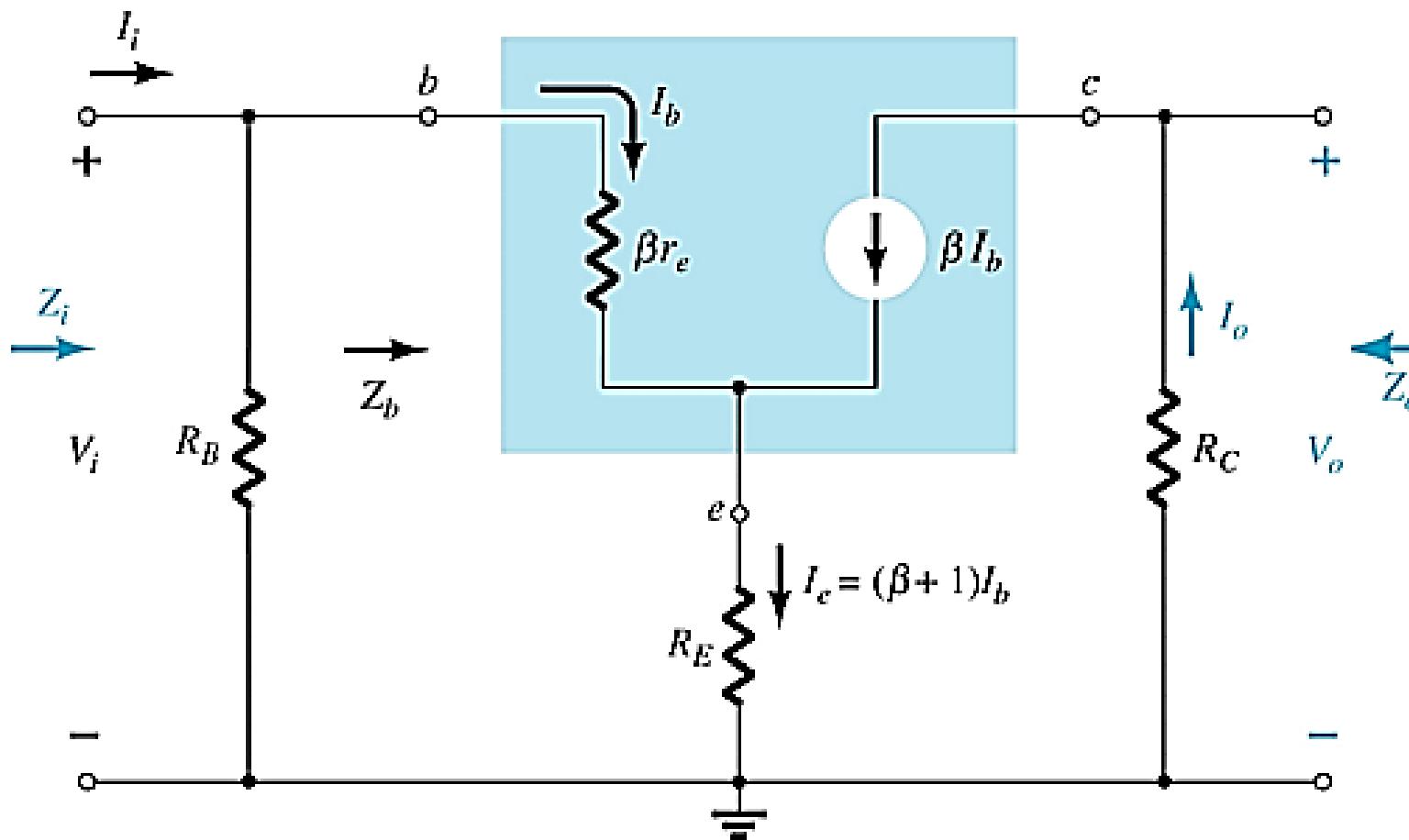
$$A_i = \frac{I_o}{I_i} \approx \frac{\beta R'}{R' + \beta r_e} \Big| r_o \geq 10R_C$$

$$A_i = \frac{I_o}{I_i} \approx \beta \Big| r_o \geq 10R_C, R' \geq 10\beta r_e$$

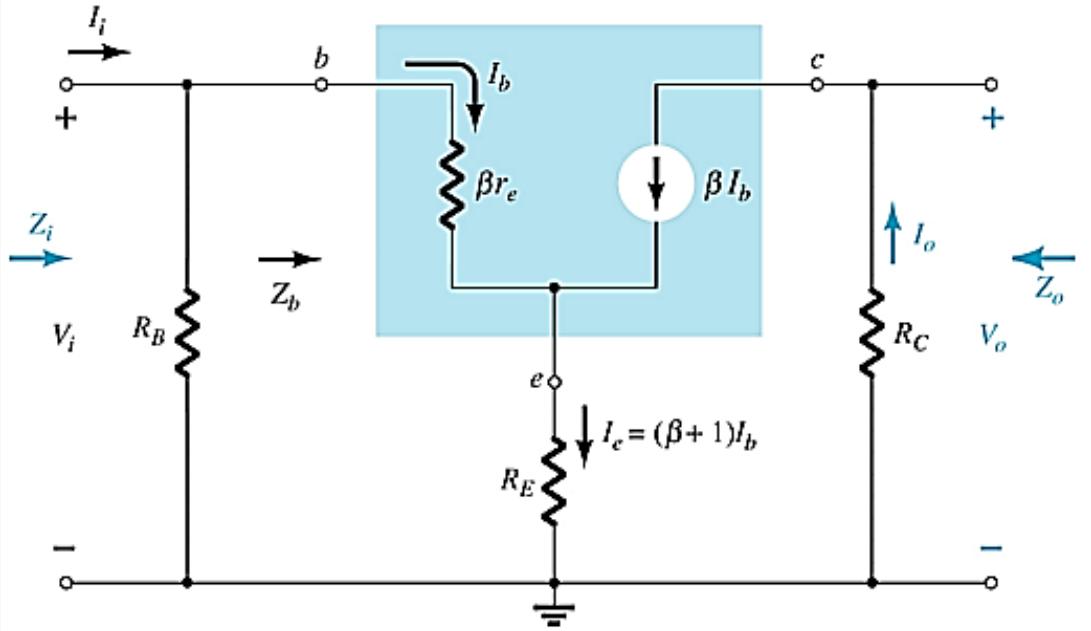
# Common-Emitter Emitter-Bias Configuration



## Equivalent Model



**Emitter-Bias Configuration**



- Input impedance:

$$Z_i = R_B \parallel Z_b$$

$$Z_b = \beta r_e + (\beta + 1)R_E$$

$$Z_b \approx \beta(r_e + R_E)$$

$$Z_b \approx \beta R_E$$

- Voltage gain:

$$A_v = \frac{V_o}{V_i} = -\frac{\beta R_C}{Z_b}$$

$$A_v = \frac{V_o}{V_i} = -\frac{R_C}{r_e + R_E} \quad | Z_b = \beta(r_e + R_E)$$

$$A_v = \frac{V_o}{V_i} \approx -\frac{R_C}{R_E} \quad | Z_b \approx \beta R_E$$

- Output impedance:

$$Z_o = R_C$$

- Current gain:

$$A_i = \frac{I_o}{I_i} = \frac{\beta R_B}{R_B + Z_b}$$