

Structural Mechanics (1)

Week No-06 Part-01

Analysis of Indeterminate Structures - Force Method



- Determinate Structures vs. Determinate Structures
- Analysis of Indeterminate Structures.
- Structures with single Degree of Indeterminacy (Beams & Frames)
- Structures with single Degree of Indeterminacy (Trusses: Int. & Ext.)

STRUCTURES

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are classified from the analysis point of view to

DETERMINATE

INDETERMINATE

To predict the performance of a structure, its response elements such like sup. reactions, internal forces, stresses, deflections, strain, to external actions Loads, sup. settlement, temp. changes & fabric. errors, must be determined.



Response elements are not separable

Forces: support reactions & internal forces, then stresses, are determined by equilibrium equations

support reactions & internal forces number is greater than the available equilibrium equations

Deformations: deflections & Strains, are determined after knowing the first group

additional relationships based on the geometry of deformation of structures, are needed

INDETERMINATE STRUCTURES



Advantages

greater overall factor of safety

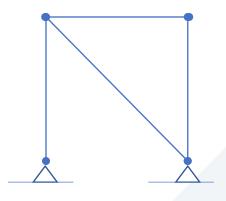
- 1. Smaller Stresses
- 2. Greater Stiffness
- 3. Redundancies

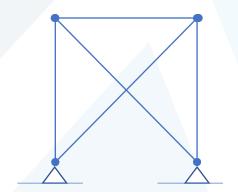
Disadvantages

more sensitive to secondary effects

- 1. Fabrication errors
- 2. Temperature changes
- 3. Support settlements







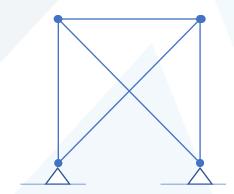
Statically Determinate



Geometric changes cause indirect stresses

1. Fabrication errors:



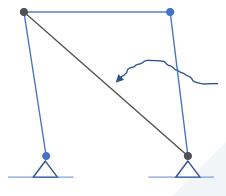


Statically Determinate

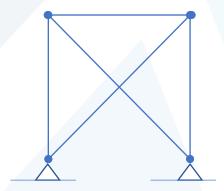


Geometric changes cause indirect stresses

1. Fabrication errors:



If this is accidentally Fabricated too long... All joints just move to New positions

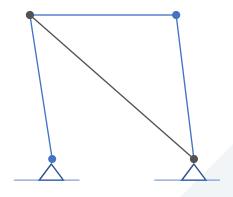


Statically Determinate

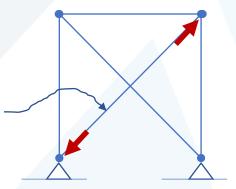


Geometric changes cause indirect stresses

1. Fabrication errors:



If this is accidentally Fabricated too long...

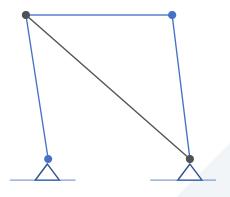


Statically Determinate



Geometric changes cause indirect stresses

1. Fabrication errors:

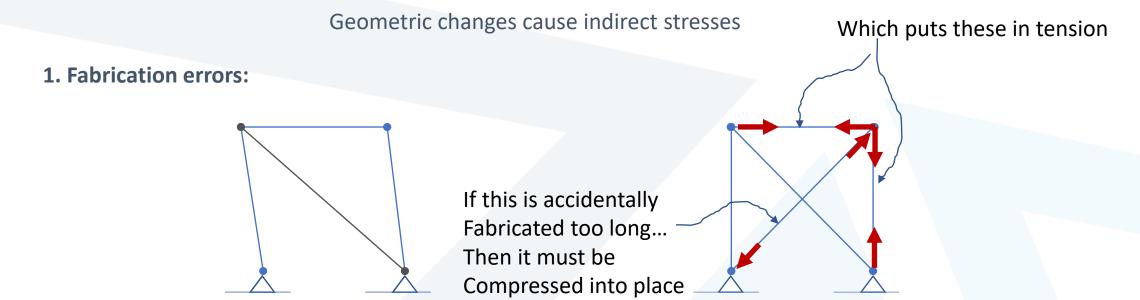


If this is accidentally
Fabricated too long...
Then it must be
Compressed into place

ce

Statically Determinate



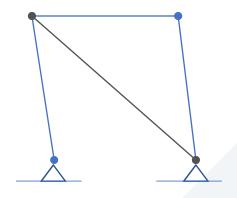


Statically Determinate

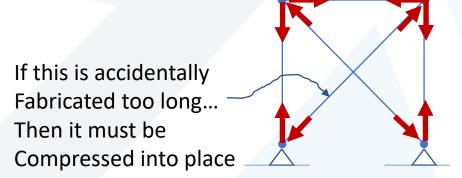


Geometric changes cause indirect stresses

1. Fabrication errors:



Which puts forces on all members

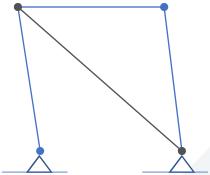


Statically Determinate



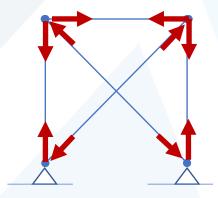
Geometric changes cause indirect stresses

1. Fabrication errors:



No Stresses. Members go together.

Statically Determinate

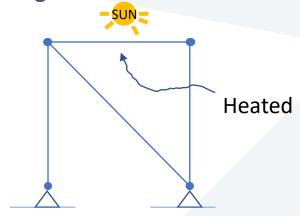


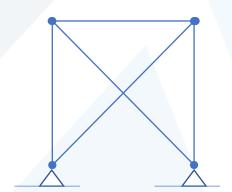
Members must be forced to fit.



Geometric changes cause indirect stresses

2. Temperature Changes:



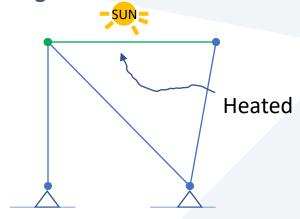


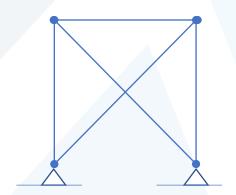
Statically Determinate



Geometric changes cause indirect stresses

2. Temperature Changes:





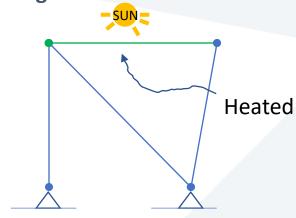
No Stresses. Positions just change

Statically Determinate



Geometric changes cause indirect stresses

2. Temperature Changes:



Heated

Joints restricted by truss-action

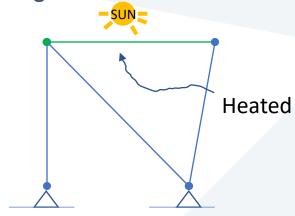
No Stresses. Positions just change

Statically Determinate



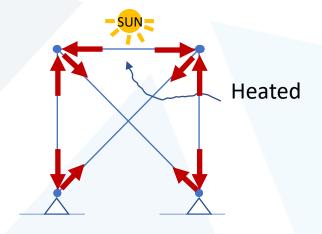
Geometric changes cause indirect stresses

2. Temperature Changes:



No Stresses. Positions just change

Statically Determinate

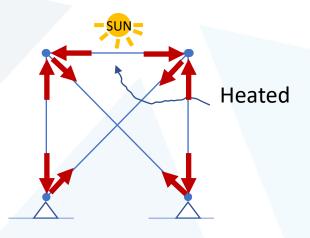


Thermal causes stresses









Thermal causes stresses

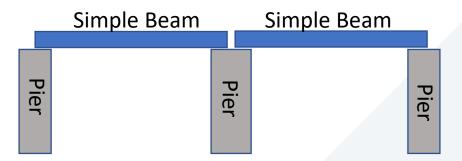








Geometric changes cause indirect stresses

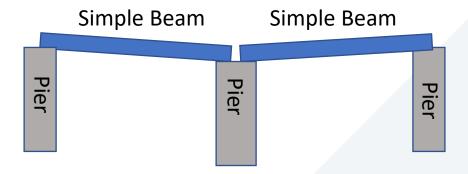


Statically Determinate



Geometric changes cause indirect stresses

3. Foundation Settlement:



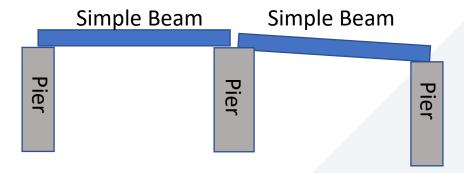
Any Settlement: No Curvature. No moment

Statically Determinate



Geometric changes cause indirect stresses

3. Foundation Settlement:



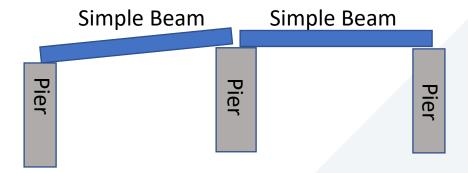
Any Settlement: : No Curvature. No moment

Statically Determinate



Geometric changes cause indirect stresses

3. Foundation Settlement:



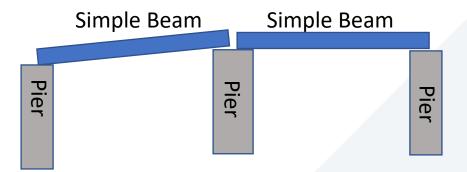
Any Settlement: : No Curvature. No moment

Statically Determinate



Geometric changes cause indirect stresses

3. Foundation Settlement:



Continuous Beam

Pier

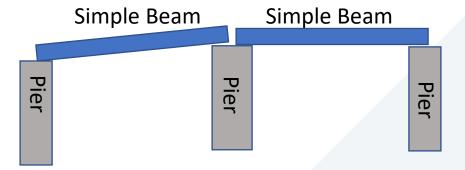
Any Settlement: : No Curvature. No moment

Statically Determinate



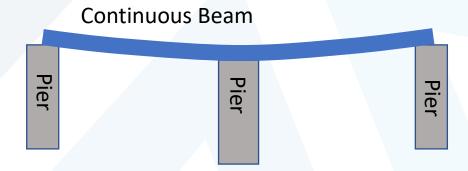
Geometric changes cause indirect stresses

3. Foundation Settlement:



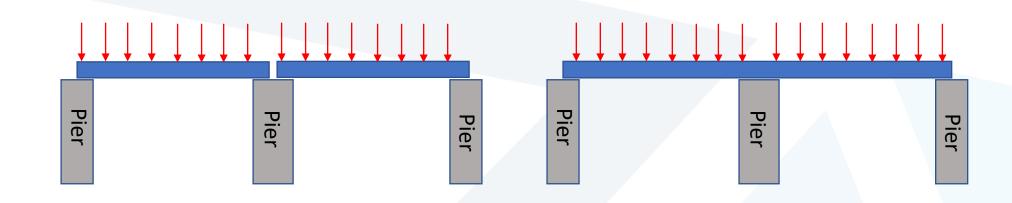
Any Settlement: : No Curvature. No moment

Statically Determinate



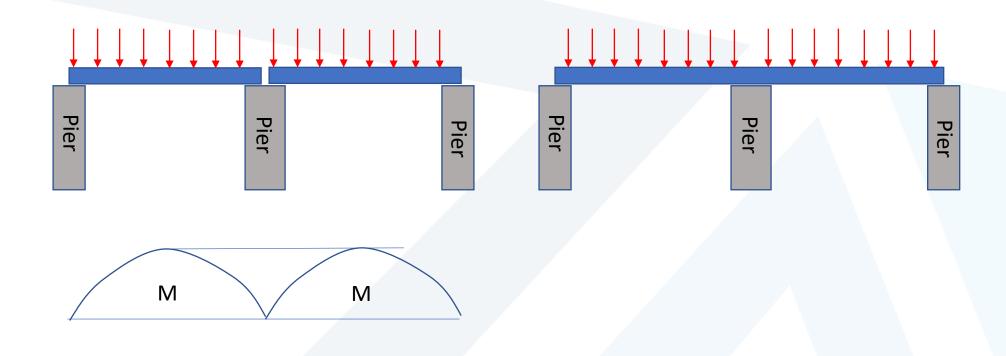
Any Settlement: : Curvature! Moment!





Statically Determinate

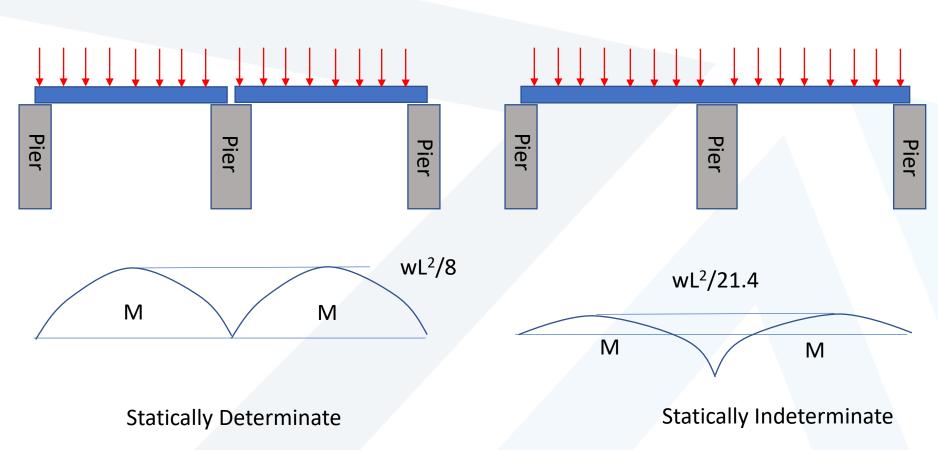




Statically Determinate

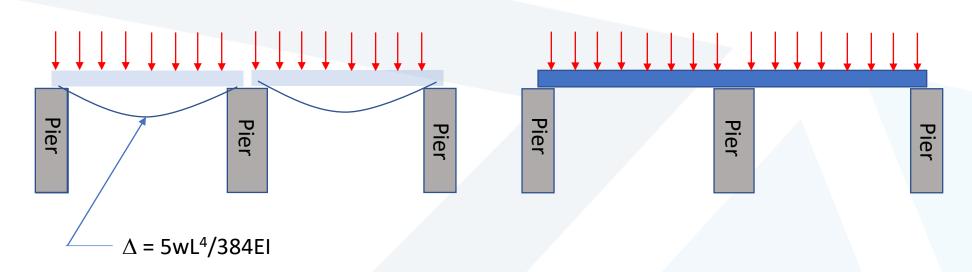








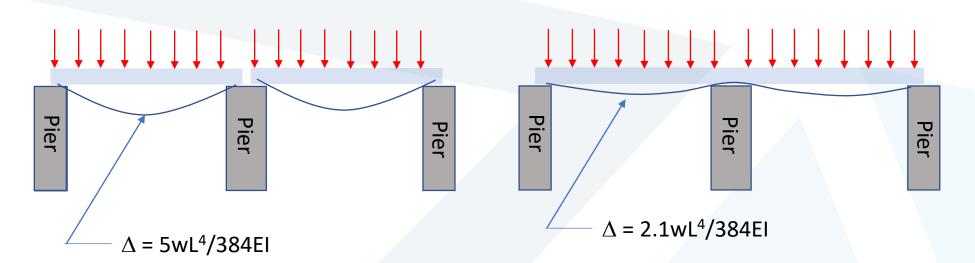
2. Greater Stiffness:



Statically Determinate

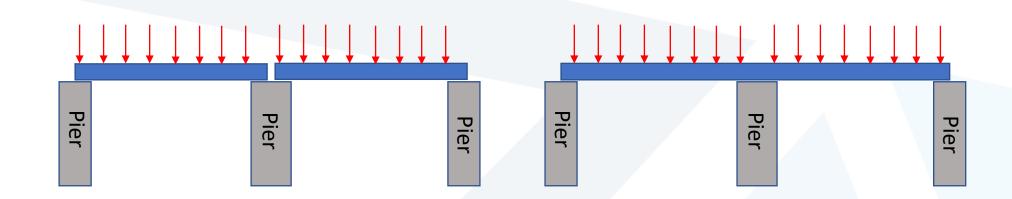


2. Greater Stiffness:



Statically Determinate





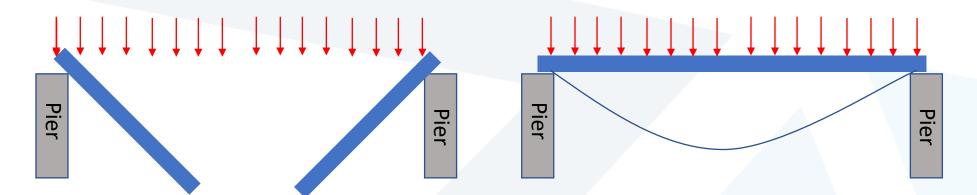
A catastrophic event eliminates the middle pier

Statically Determinate: $DOI_s = 0$

Statically Indeterminate: DOI_s = 1



2. Greater Robustness: - May survive redundant loss of massive overload



Will NOT Survive (zero redundancy)

MAY Survive (if the beam can take a Substantial increase in moment)

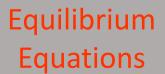
A catastrophic event eliminates the middle pier

Statically Determinate: $DOI_s = 0$

Statically Indeterminate: $DOI_s = 1$

ANALYSIS OF INDETERMINATE STRUCTURES

Three Pillars of Mechanics



Constitutive Equations or Behavior Lows

Compatibility Equations

the response elements

(support reactions, internal forces, stresses, deflections, strain) are classified into primary & secondary unknowns

Force methods

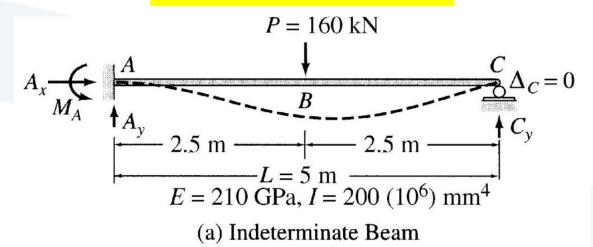
Primary unknowns are reactions & Internal forces
Secondary unknowns are displacements: deflections & rotations (slopes)

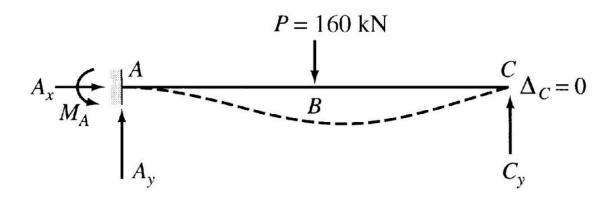
Displacement methods

Primary unknowns are
displacements: deflections &
rotations (slopes) Secondary
unknowns are reactions &
Internal forces



illustrative example





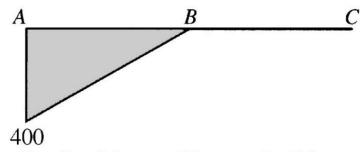
(b) Primary Beam Subjected to External Loading and Redundant C_y



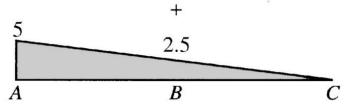
Compatibility

Equation

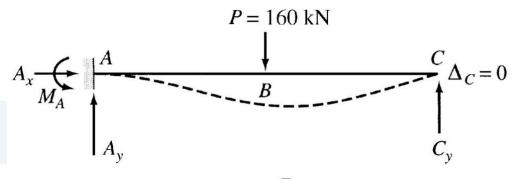
$$\Delta_C = \Delta_{CO} + f_{CC} C_v = 0$$

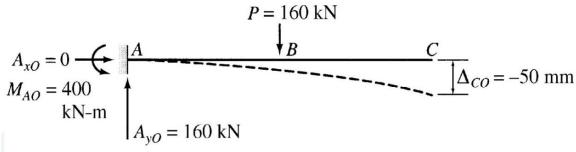


Bending Moment Diagram for Primary Beam Due to External Loading (kN-m)

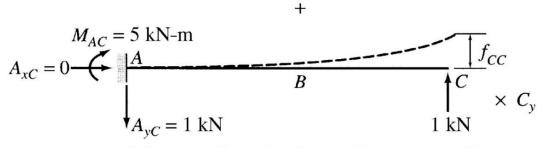


Bending Moment Diagram for Primary Beam Due to Unit Value of C_y (kN-m/kN





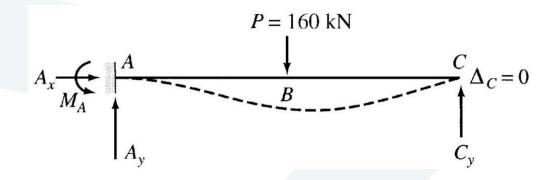
(c) Primary Beam Subjected to External Loading



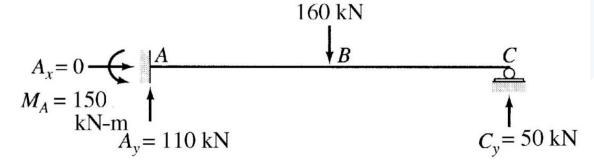
(d) Primary Beam Loaded with Redundant C_v

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Compatibility Equation



$$C_y = -\Delta_{CO}/f_{CC} = 5P/16 = 50 \text{ kN}$$

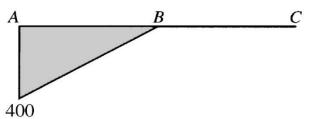


(e) Support Reactions for Indeterminate Beam

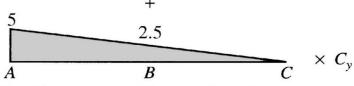
By the method of section & using the equilibrium equations, the BM & SF diagrams can be found



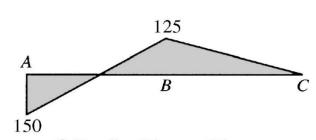
Or, the BM diagram can be found using the superposition principle as



Bending Moment Diagram for Primary Beam Due to External Loading (kN-m)



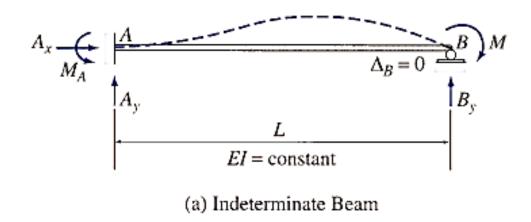
Bending Moment Diagram for Primary Beam Due to Unit Value of $C_y(kN-m/kN)$



(f) Bending Moment Diagram for Indeterminate Beam (kN-m)

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Example-01: Compute the support then draw the BM & SF diagrams for the following beam.



SOLUTION: The beam is statically indeterminate to degree one. Select B_y as the redundant. Draw the two determinate frames $(S_0) & (S_1)$



Example-01: Compute the support then draw the BM & SF diagrams for the following beam.



(b) Primary Beam Subjected to External Moment M

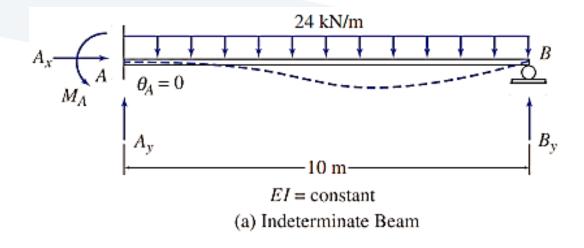
(c) Primary Beam Loaded with Redundant B_v

The compatibility equation is

$$\Delta_{0B} + B_y f_{BB} = 0$$



Example-02: Compute the support then draw the BM & SF diagrams for the following beam.

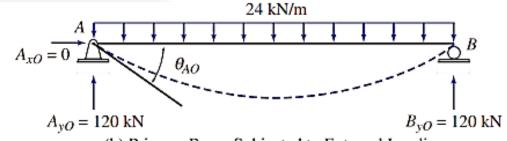


SOLUTION: The beam is statically indeterminate to degree one. Select M_A as the redundant. Draw the two determinate frames $(S_0) & (S_1)$



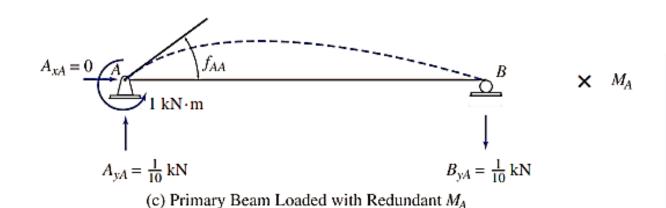
Example-02: Compute the support then draw the BM & SF diagrams for the following beam.

 S_0



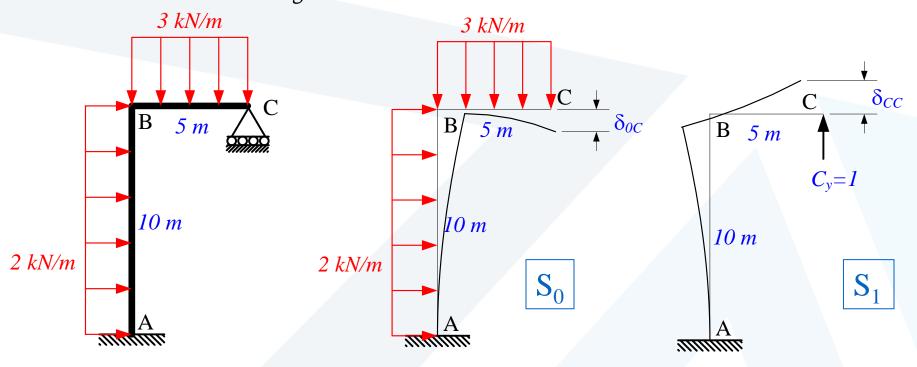
(b) Primary Beam Subjected to External Loading

 $\overline{\mathbf{S}_1}$





Compute the support reactions in the frame. E = 200 GPa, $I_c = 10^6 \text{ mm}^4$ for the column & $I_b = 2I_c$, for the beam. Then draw the BM & SF diagrams



SOLUTION: The frame is statically indeterminate to degree one. Select C_y as the redundant. Draw the two determinate frames $(S_0) & (S_1)$

The compatibility equation is

$$\delta_{0C} + C_y \delta_{CC} = 0$$



Segment	FBD in S ₀	$M_0(x)$	FBD in S ₁	$m_{\rm C}(x)$
СВ	3 kN/m		$m_C(x)$	
$0 \le x \le 5$	$M_0(x)$	$-3x^2/2$	C	χ
<i>2EI</i> is	C	-3x 12	x	\mathcal{A}
constant	$V_0(x)$		$V_C(x)$	
AB	$M_0(x)$ $V_0(x)$		$m_C(x)$	
$0 \le x \le 10$				
EI is	*	$-x^2+20x-137.5$	X X	_
constant	2 kN/m			5
	137.5 A 20		A	
1 (2	15		5 1	

$$\delta_{0C} = \frac{1}{2EI} \int_0^5 \left(-\frac{3x^2}{2} \right) (x) dx + \frac{1}{EI} \int_0^{10} (-x^2 + 20x - 137.5)(5) dx = -\frac{234.375}{2EI} - \frac{3541.67}{EI} = -\frac{3658.85}{EI}$$

$$\delta_{CC} = \frac{1}{2EI} \int_0^5 x^2 dx + \frac{1}{EI} \int_0^{10} 25 dx = \frac{270.833}{EI} \implies C_y = 13.5 \text{ kN}$$



Computing the reactions

$$\uparrow + \sum_{y} F_{y} = 0 \Rightarrow A_{y} + 13.5 - 15 = 0 \Rightarrow A_{y} = 1.5kN$$

$$\sum_{x}^{+} F_x = 0 \Rightarrow A_x + 20 = 0 \Rightarrow A_x = -20kN = 20kN(\leftarrow)$$

$$(\downarrow\uparrow+)\sum M_A = 0 \Rightarrow M_A - (5)20 - (2.5)15 + (5)13.5 = 0 \Rightarrow M_A = 70\text{kN.m}$$

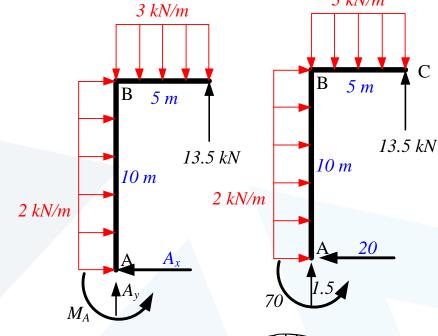


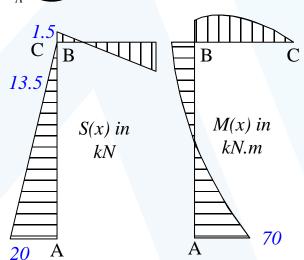
In the segment AB: 0 < x < 10,

$$M(x) = -x^2 + 20x - 70\&S(x) = -2x + 20$$

In Segment CB: 0 < x < 5,

$$M(x) = -(3/2)x^2 + (27/2)x&S(x) = 3x - 13.5$$





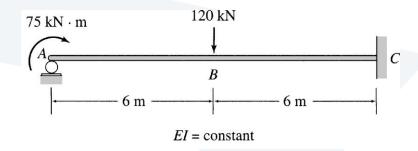


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Homework



Pr.01: Determine the reactions and draw the shear and bending moment diagrams for the beam shown using force method. Select the reaction at the roller support to be the redundant.



Pr.02: Determine the reactions and draw the shear and bending moment diagrams for the frame shown using force method. Select the reaction at the roller support to be the redundant.

