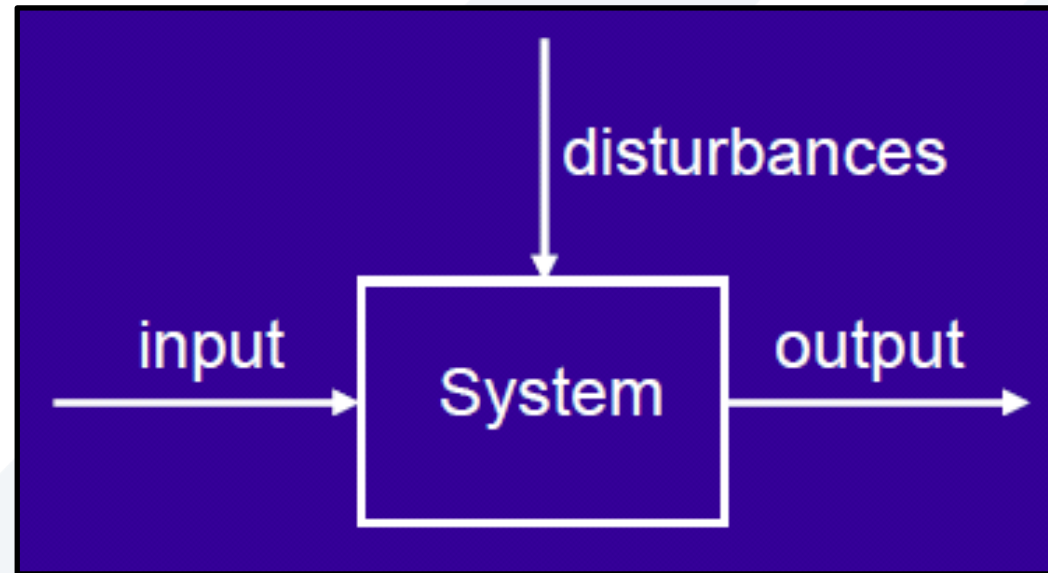


## Mathematical Techniques to Analyze System Responses



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## INTRODUCTION

An input that changes at a constant rate is modeled by the ramp function. The step function models an input that rapidly reaches a constant value, while the rectangular pulse function models a constant input that is suddenly removed. The *impulse* is similar to the pulse function, but it models an input that is suddenly applied and removed after a *very short* time. The impulse, which is a mathematical function only and has no physical counterpart, has an infinite magnitude for an infinitesimal time.

## THE STEP FUNCTION APPROXIMATION

The step function is an approximate description of an input that can be switched on in a time interval that is very short compared to the time constant of the system. A good example of a step input is the voltage applied to a circuit due to the sudden closure of a switch.

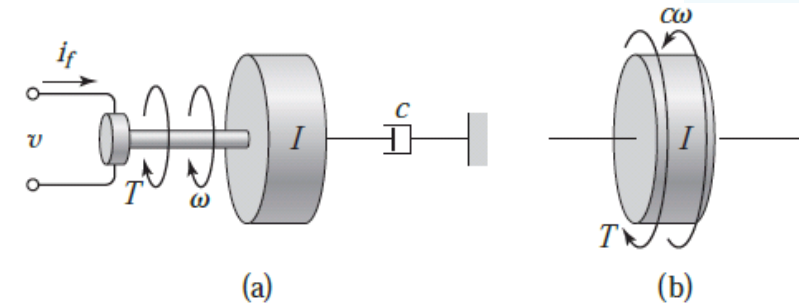
## Example

A certain rotational system has an inertia  $I = 50 \text{ kg} \cdot \text{m}^2$  and a viscous damping constant  $c = 10 \text{ N} \cdot \text{m} \cdot \text{s}/\text{rad}$ . The torque  $T(t)$  is applied by an electric motor. From the free body diagram shown in part (b) of the figure, the equation of motion is

$$50 \frac{d\omega}{dt} + 10\omega = T(t) = K_f i_f \quad (1)$$

The model of the motor's field current  $i_f$  in amperes is

$$0.001 \frac{di_f}{dt} + 5i_f = v(t) \quad (2)$$



where  $v(t)$  is the voltage applied to the motor. The motor torque constant is  $K_T = 25 \text{ N} \cdot \text{m}/\text{A}$ .

Suppose the applied voltage is  $10 \text{ V}$ . Determine the steady-state speed of the inertia and estimate the time required to reach that speed.

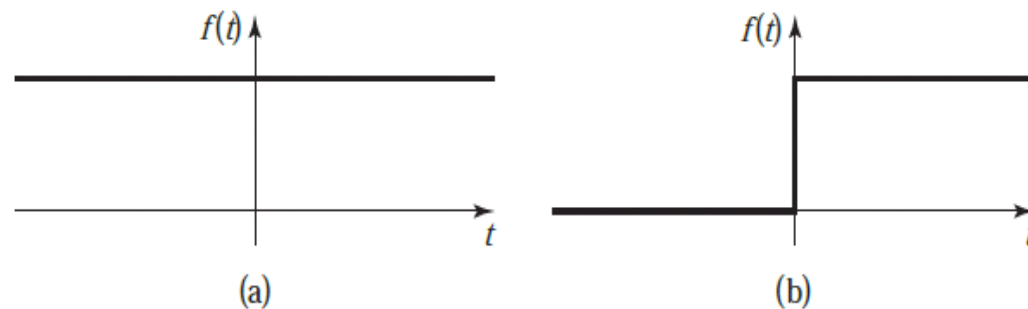
## Solution

From equation (2) we see that the time constant of the motor circuit is  $0.001/5 = 2 \times 10^{-4}$  s. Thus the current will reach a steady-state value of  $10/5 = 2$  A in approximately  $4(2 \times 10^{-4}) = 8 \times 10^{-4}$  s. The resulting steady-state torque is  $K_T(2) = 25(2) = 50$  N · m.

From equation (1) we find the time constant of the rotational system to be  $50/10 = 5$  s. Since this is much larger than the time constant of the circuit ( $2 \times 10^{-4}$  s), we conclude that the motor torque may be modeled as a step function. The magnitude of the step function is 50 N · m. The steady-state speed is  $\omega = 50/10 = 5$  rad/s, and therefore it will take approximately  $4(5) = 20$  s to reach this speed.

## STEP INPUTS VERSUS CONSTANT INPUTS

Consider the two input functions shown in Figure. The one shown in part (a) is constant, whereas in part (b) the input is a step function. For the constant input, the derivative is always zero, but for the step input the derivative is an impulse function, which is infinite at  $t = 0$  and zero elsewhere. So if we are interested in finding the response of a model only for  $t \geq 0$ , then we can conclude that it does not matter whether we model the input as a constant or as a step, *as long as the model does not contain any time derivatives of the input.*



## STEP RESPONSE WITH AN INPUT DERIVATIVE

The general form of the first-order linear model is

$$m\dot{v} + cv = b\dot{f}(t) + f(t)$$

whose transfer function is of the form

$$\frac{V(s)}{F(s)} = \frac{bs + 1}{ms + c}$$

The presence of an input derivative is indicated by an  $s$  in the numerator of the transfer function. Such a transfer function is said to have *numerator dynamics*.

If  $f(t)$  is a step function of magnitude  $F$ , then  $F(s) = F/s$  and  $f(0) = 0$ ,



$$V(s) = \frac{mv(0) + bF}{ms + c} + \frac{F}{s(ms + c)}$$

which gives

$$v(t) = \left[ v(0) + \frac{bF}{m} \right] e^{-ct/m} + \frac{F}{c} (1 - e^{-ct/m})$$

we see that the effect of the  $b\dot{f}$  term is to increase the effective initial value of  $v(t)$  by the amount  $bF/m$ .

## IMPULSE RESPONSE

The impulse response of  $m\dot{v} + cv = f(t)$  is found as follows, where  $A$  is the impulse *strength*, or the area under the impulse versus time curve.

$$msV(s) - mv(0) + cV(s) = A$$
$$V(s) = \frac{mv(0) + A}{ms + c} = \frac{v(0) + A/m}{s + c/m}$$
$$v(t) = \left[ v(0) + \frac{A}{m} \right] e^{-ct/m}$$

We can see that the effect of the impulse is to increase the effective initial condition by  $A/m$ .

Because  $\dot{f}(t)$  is undefined if  $f(t)$  is an impulse, we do not consider the impulse response of the equation  $m\dot{v} + cv = f(t) + b\dot{f}(t)$ .

## RAMP RESPONSE AND THE TIME CONSTANT

We can obtain the response of the general equation  $\tau \dot{v} + v = f(t)$  to the ramp input  $f(t) = mt$  as follows. Setting  $v(0) = 0$  and transforming the equation with  $F(s) = m/s^2$  gives

$$\tau s V(s) + V(s) = F(s) = \frac{m}{s^2}$$

or

$$V(s) = \frac{m}{s^2(\tau s + 1)} = \frac{m}{s^2} - \frac{m\tau}{s} + \frac{m\tau}{s + 1/\tau}$$

The inverse transforms give

$$v(t) = m(t - \tau) + m\tau e^{-t/\tau}$$

The response is in steady state after approximately  $t = 4\tau$ . At steady state,  $v(t) = m(t - \tau)$ , so the response is parallel to the input but lags behind it by a time  $\tau$

Obtaining the ramp response can be tedious for higher-order systems, but sometimes we only need to find the steady-state *difference* between the input and the output.

### Example

Obtain the steady-state difference  $f(\infty) - v(\infty)$  between the input and output of the following model:  $\tau \dot{v} + v = bf(t)$ , where  $b$  is a constant and  $f(t) = mt$ . Assume that  $v(0) = 0$  and that the model is stable ( $\tau > 0$ ).

## Solution

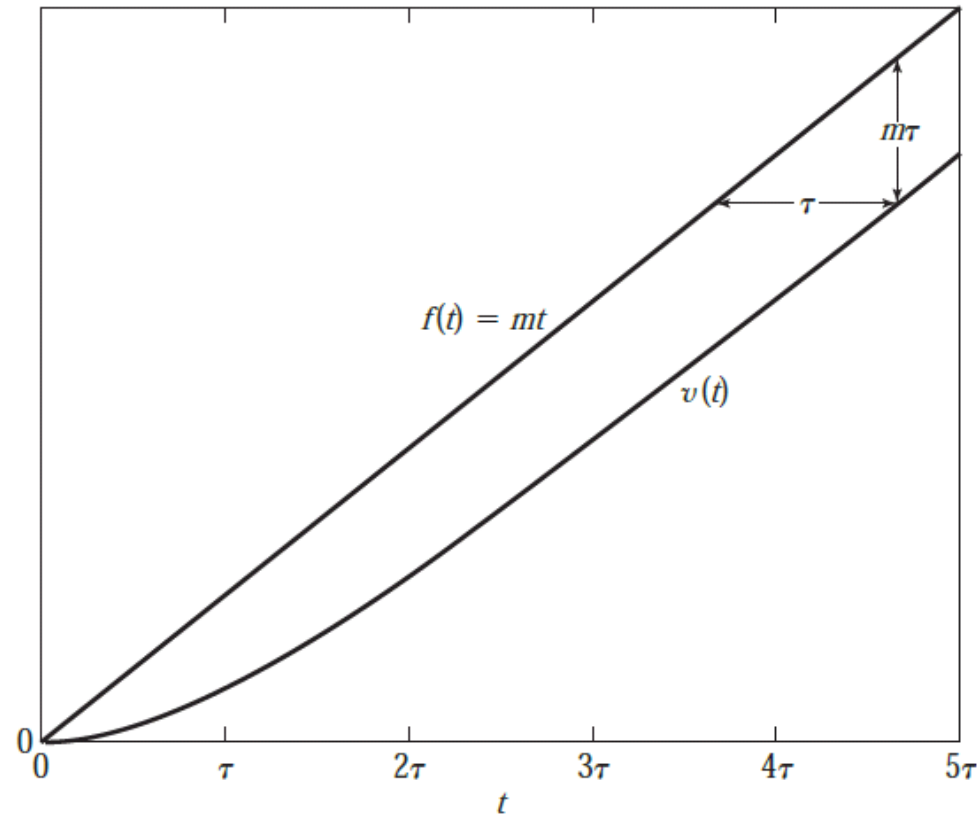
The transform of the response is

$$V(s) = \frac{b}{\tau s + 1} F(s) = \frac{b}{\tau s + 1} \frac{m}{s^2}$$

Use this with the final value theorem to find the steady-state difference:

$$\begin{aligned} f(\infty) - v(\infty) &= \lim_{s \rightarrow 0} [sF(s)] - \lim_{s \rightarrow 0} [sV(s)] = \lim_{s \rightarrow 0} s[F(s) - V(s)] \\ &= \lim_{s \rightarrow 0} s \left( \frac{m}{s^2} - \frac{b}{\tau s + 1} \frac{m}{s^2} \right) \\ &= \lim_{s \rightarrow 0} \frac{m}{s} \left( \frac{\tau s + 1 - b}{\tau s + 1} \right) \\ &= \begin{cases} \infty & b \neq 1 \\ m\tau & b = 1 \end{cases} \end{aligned}$$

Thus, the steady-state difference is infinite unless  $b = 1$ . Both the input and output approach straight lines at steady state. The preceding result shows that the lines diverge unless  $b = 1$ .



## NUMERATOR DYNAMICS AND SECOND-ORDER SYSTEM RESPONSE

For the model  $m\ddot{x} + c\dot{x} + kx = a\dot{g}(t) + bg(t)$ , the effect on the step response of the numerator dynamics coefficient  $a$  is to change the formulas for the constants  $A_1$  and  $A_2$  in Table for the real roots cases, and the formulas for the amplitude  $B$  and angle  $\phi$  for the complex roots case.

### Unit step response of a stable second-order model

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Model:  $m\ddot{x} + c\dot{x} + kx = u_s(t)$

Initial conditions:  $x(0) = \dot{x}(0) = 0$

Characteristic roots:  $s = \frac{-c \pm \sqrt{c^2 - 4mk}}{2m} = -r_1, -r_2$

1. Overdamped case ( $\zeta > 1$ ): distinct, real roots:  $r_1 \neq r_2$

$$x(t) = A_1 e^{-r_1 t} + A_2 e^{-r_2 t} + \frac{1}{k} = \frac{1}{k} \left( \frac{r_2}{r_1 - r_2} e^{-r_1 t} - \frac{r_1}{r_1 - r_2} e^{-r_2 t} + 1 \right)$$

2. Critically damped case ( $\zeta = 1$ ): repeated, real roots:  $r_1 = r_2$

$$x(t) = (A_1 + A_2 t) e^{-r_1 t} + \frac{1}{k} = \frac{1}{k} [(-r_1 t - 1) e^{-r_1 t} + 1]$$

3. Underdamped case ( $0 \leq \zeta < 1$ ): complex roots:  $s = -\zeta \omega_n \pm j \omega_n \sqrt{1 - \zeta^2}$

$$x(t) = B e^{-t/\tau} \sin(\omega_n \sqrt{1 - \zeta^2} t + \phi) + \frac{1}{k}$$

$$= \frac{1}{k} \left[ \frac{1}{\sqrt{1 - \zeta^2}} e^{-\zeta \omega_n t} \sin(\omega_n \sqrt{1 - \zeta^2} t + \phi) + 1 \right]$$

$$\phi = \tan^{-1} \left( \frac{\sqrt{1 - \zeta^2}}{\zeta} \right) + \pi \quad (\text{third quadrant})$$

Time constant:  $\tau = 1/\zeta \omega_n$

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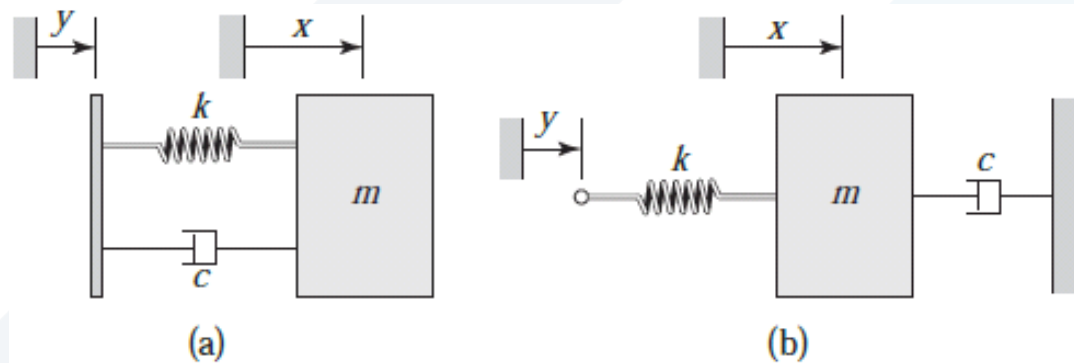


For example, consider the two systems shown in Figure for  $m = 1$ ,  $c = 6$ , and  $k = 8$ . The model for part (a) of the figure is  $\ddot{x} + 6\dot{x} + 8x = 6\dot{y} + 8y(t)$ , and the unit-step response is obtained from the Laplace transform.

$$X(s) = \frac{6s + 8}{s(s^2 + 6s + 8)} = \frac{1}{s} + \frac{1}{s + 2} - \frac{2}{s + 4}$$

Thus

$$x(t) = 1 + e^{-2t} - 2e^{-4t}$$

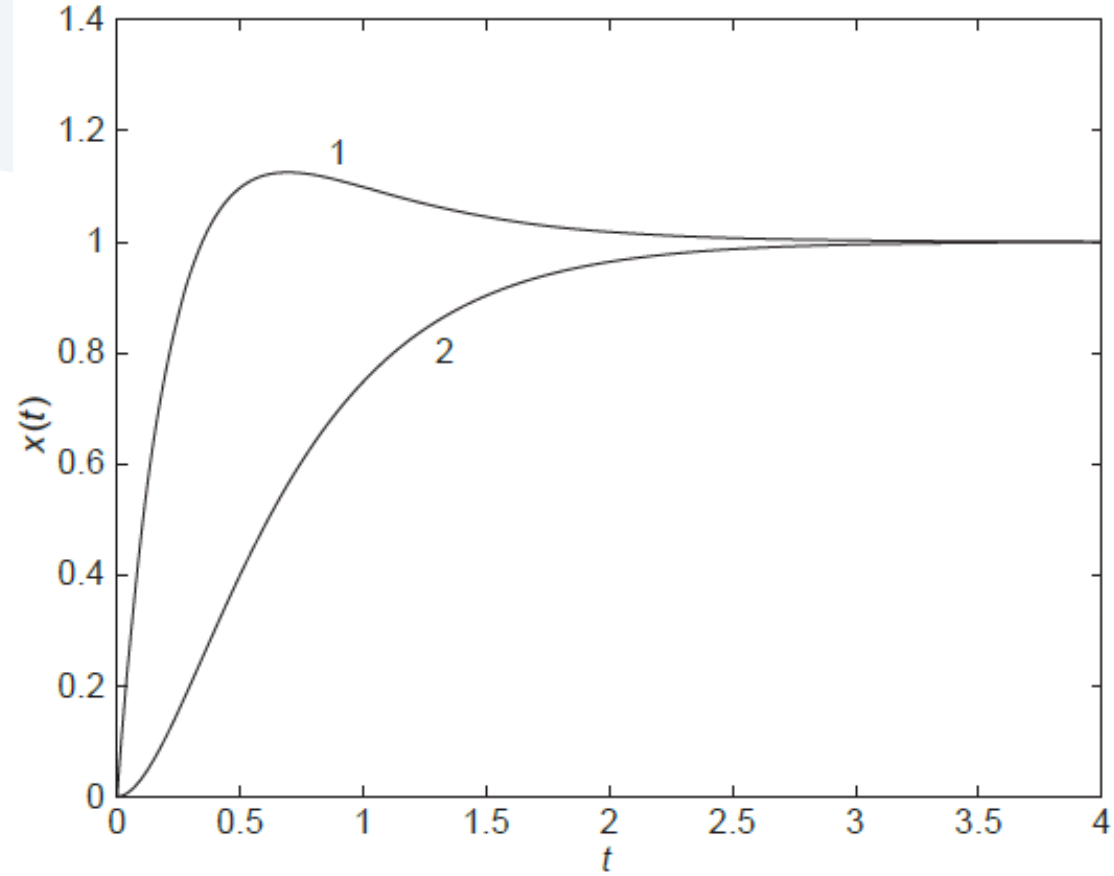


The model for part (b) of the figure is  $\ddot{x} + 6\dot{x} + 8x = 8y(t)$ , and the unit-step response is given by

$$X(s) = \frac{8}{s(s^2 + 6s + 8)} = \frac{1}{s} - \frac{2}{s + 2} + \frac{1}{s + 4}$$

$$x(t) = 1 - 2e^{-2t} + e^{-4t}$$

The responses are shown in Figure . Curve (1) corresponds to the case with numerator dynamics. We see that the numerator dynamics produces a smaller 10%–90% rise time, and causes an overshoot here, even though  $\zeta > 1$ .



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