

PRACTICAL APPLICATIONS

OF DIODES DR. BASSAM ATIEH

MANARA UNIVERSITY

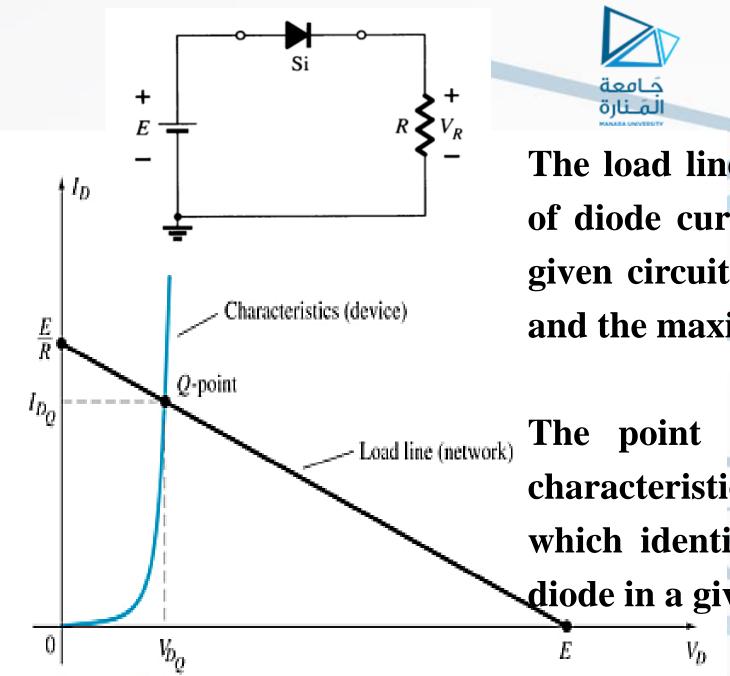
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Practical Applications

Rectifier Circuits

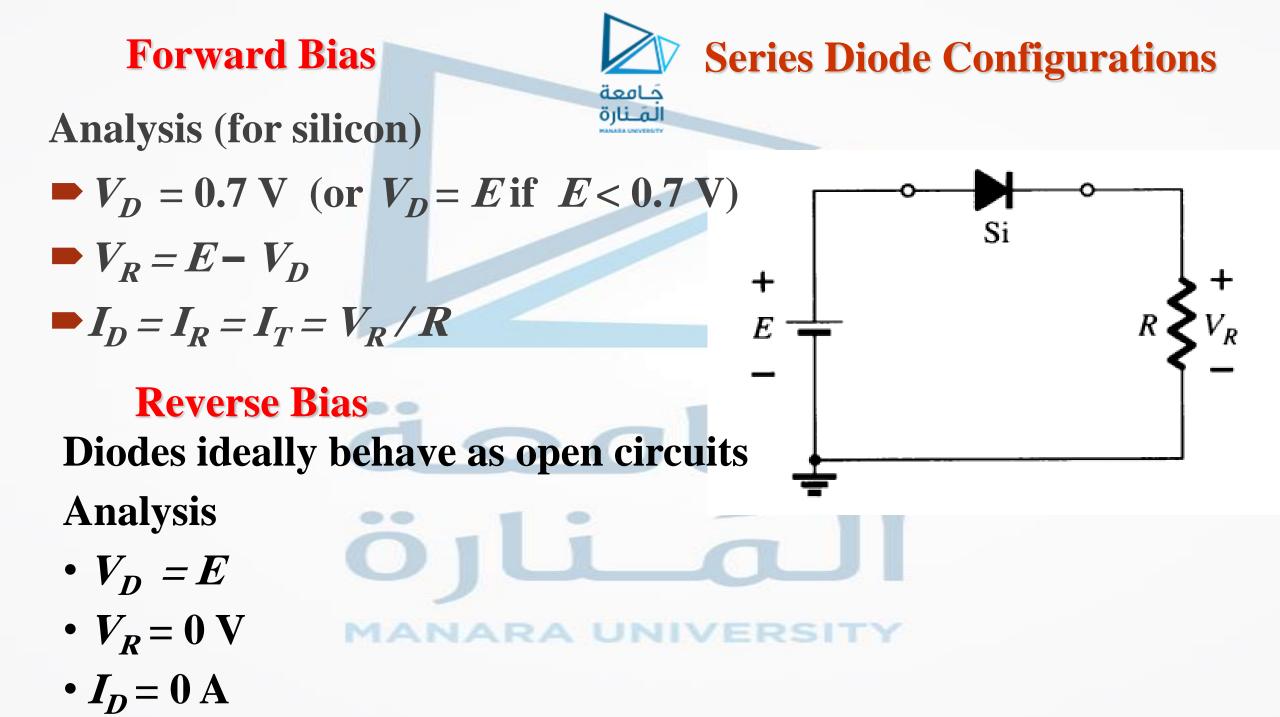
- Conversions of AC to DC for DC operated circuits
- Battery Charging Circuits
- Simple Diode Circuits
 - Protective Circuits against
 - Overcurrent •
 - Polarity Reversal
 - Currents caused by an inductive kick in a relay circuit
- **Zener Circuits**
 - Overvoltage Protection UNIVERSITY
 - Setting Reference Voltages

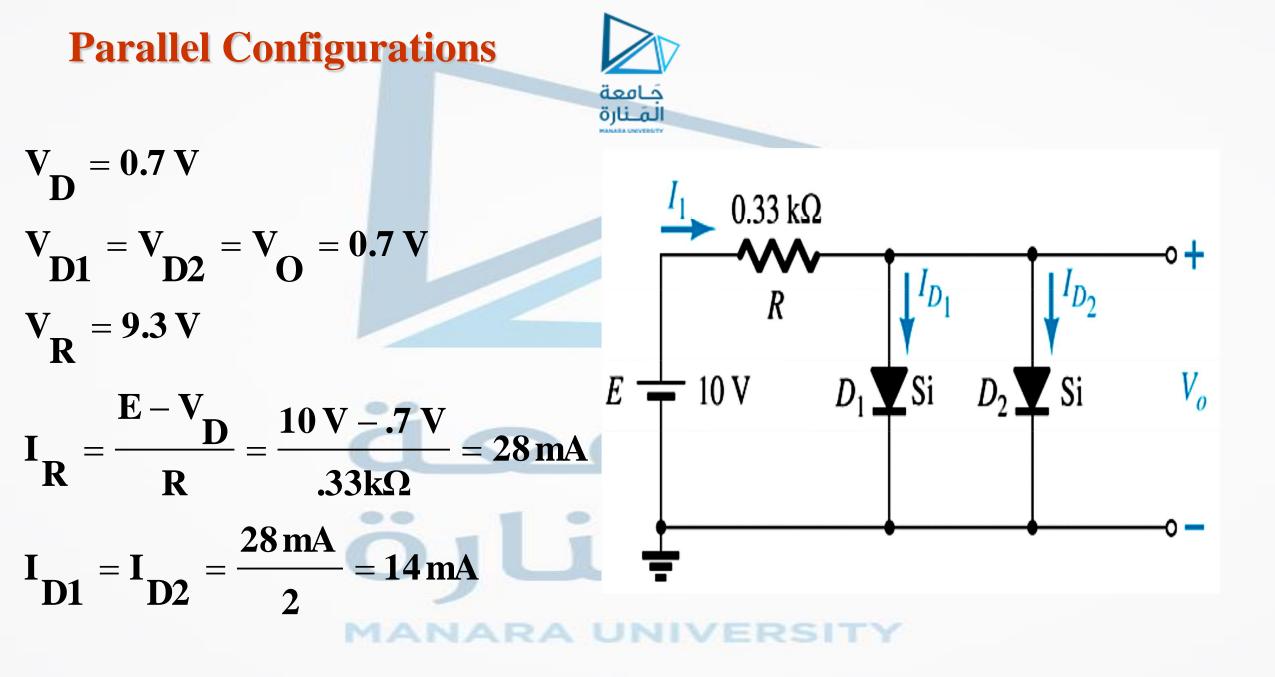


Load-Line Analysis

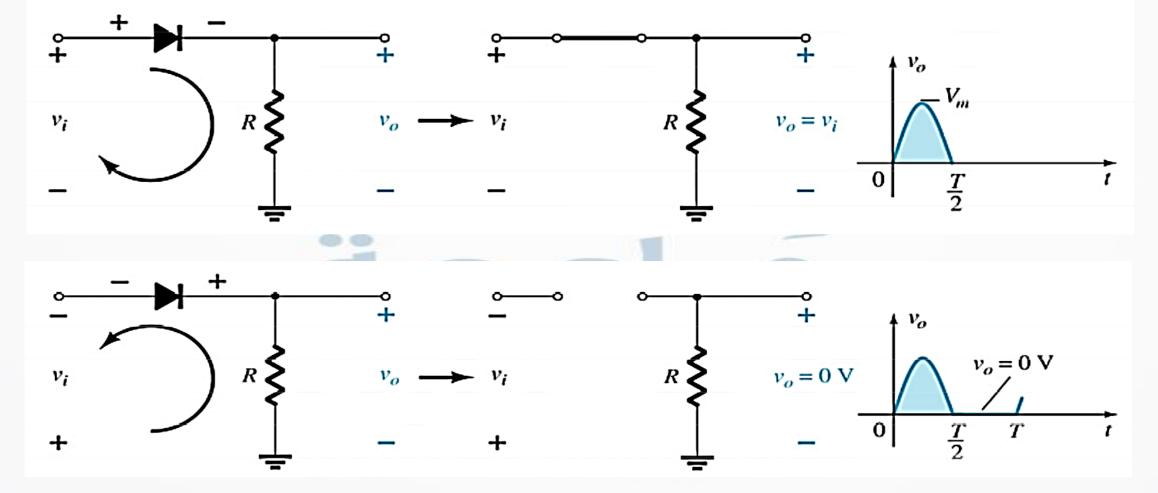
The load line plots all possible combinations of diode current (I_D) and voltage (V_D) for a given circuit. The maximum I_D equals E/R, and the maximum V_D equals E.

The point where the load line and the characteristic curve intersect is the Q-point, which identifies I_D and V_D for a particular diode in a given circuit.





Half-Wave Rectification The diode only conducts when it is forward biased, therefore only half of the AC cycle passes through the diode to the output.



The DC output voltage is $0.318 V_m$, where $V_m =$ the peak AC voltage.





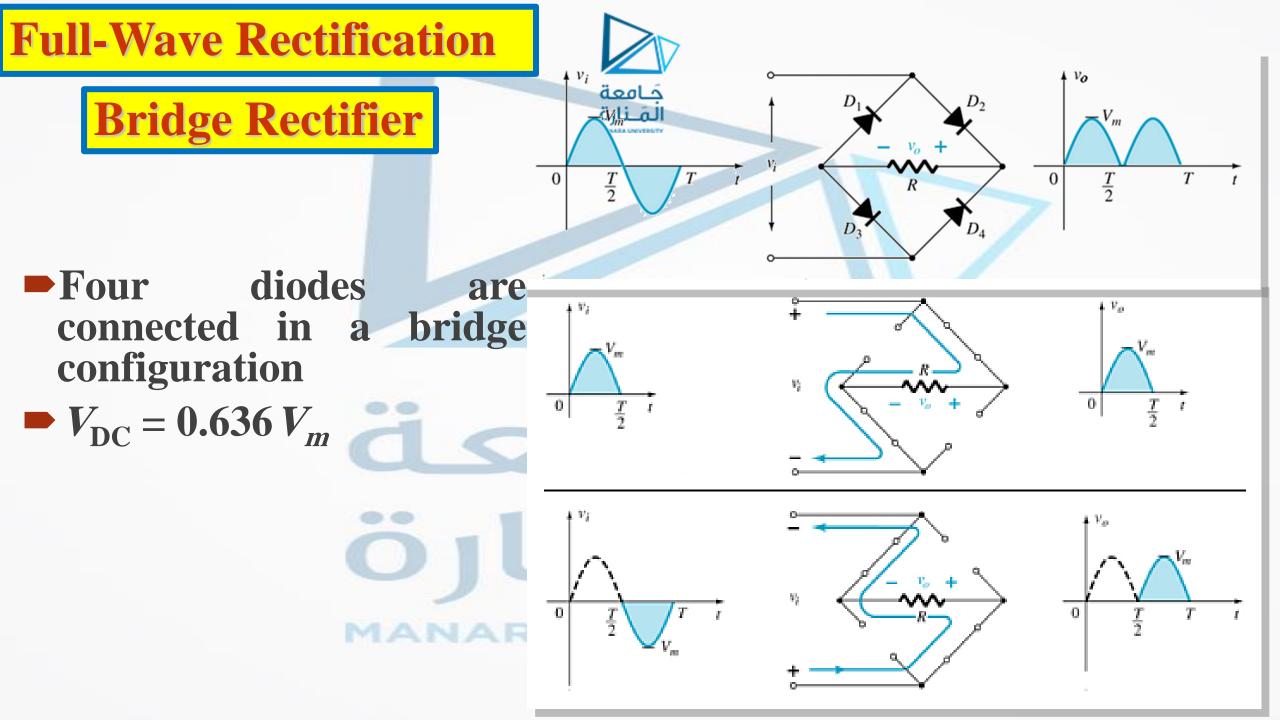
Because the diode is only forward biased for one-half of the AC cycle, it is also reverse biased for one-half cycle.

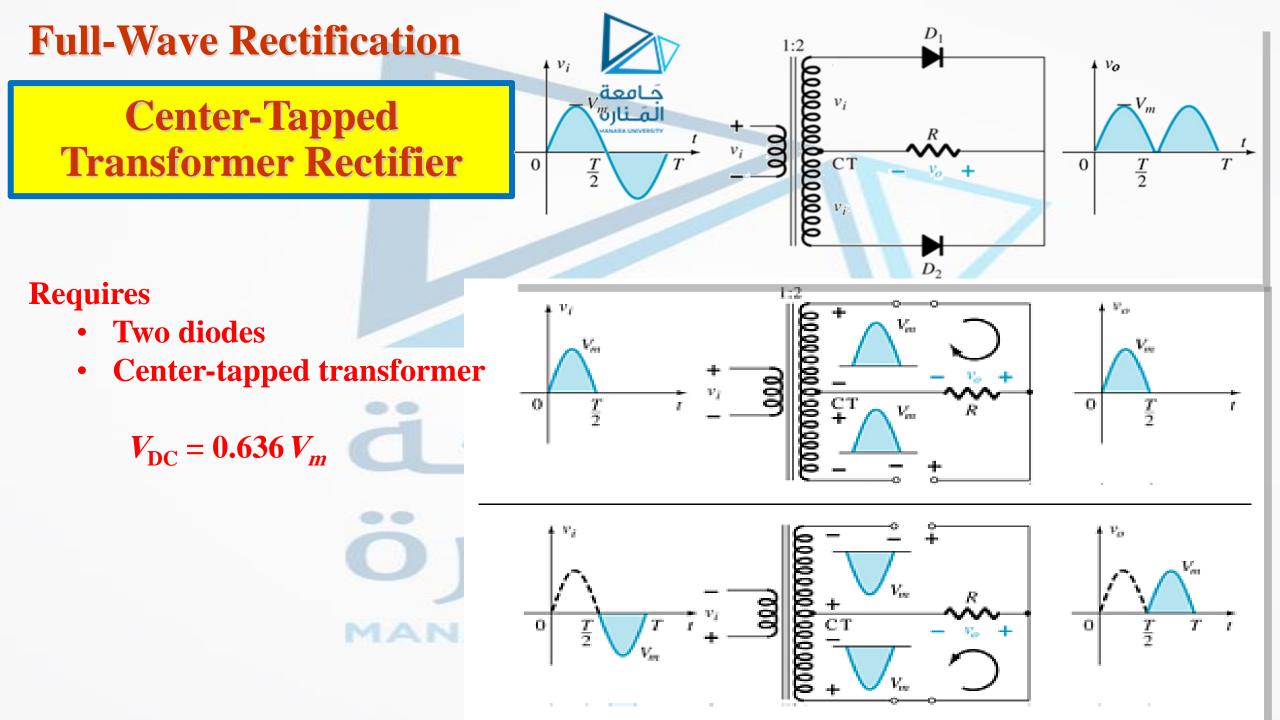
It is important that the reverse breakdown voltage rating of the diode be high enough to withstand the peak, reverse-biasing AC voltage.

PIV (or PRV) > V_m

PIV = Peak inverse voltage
PRV = Peak reverse voltage
V_m = Peak AC voltage

Full-Wave Rectification The rectification process can be improved by using a full-wave rectifier circuit. $\downarrow V_i$ **Full-wave rectification produces** V_m a greater DC output: \mathbf{O} $\frac{T}{2}$ Half-wave: Vdc = 0.318Vm v_{α} V_m Full-wave: Vdc = 0.636Vm $V_{\rm dc} = 0.636 V_m$ $\frac{T}{2}$ T t0 VE





Summary of Rectifier Circuits

Rectifier	Ideal V _{DC}	Realistic V _{DC}
Half Wave Rectifier	$V_{\rm DC} = 0.318 V_m$	$V_{\rm DC} = 0.318 V_m - 0.7$
Bridge Rectifier	$V_{\rm DC} = 0.636 V_m$	$V_{\rm DC} = 0.636 V_m - 2(0.7 \text{ V})$
Center-Tapped Transformer Rectifier	$V_{\rm DC} = 0.636 V_m$	$V_{\rm DC} = 0.636 V_m - 0.7 { m V}$

V_m = peak of the AC voltage.
In the center tapped transformer rectifier circuit, the peak
AC voltage is the transformer secondary voltage to the tap.

Smoothing of Output

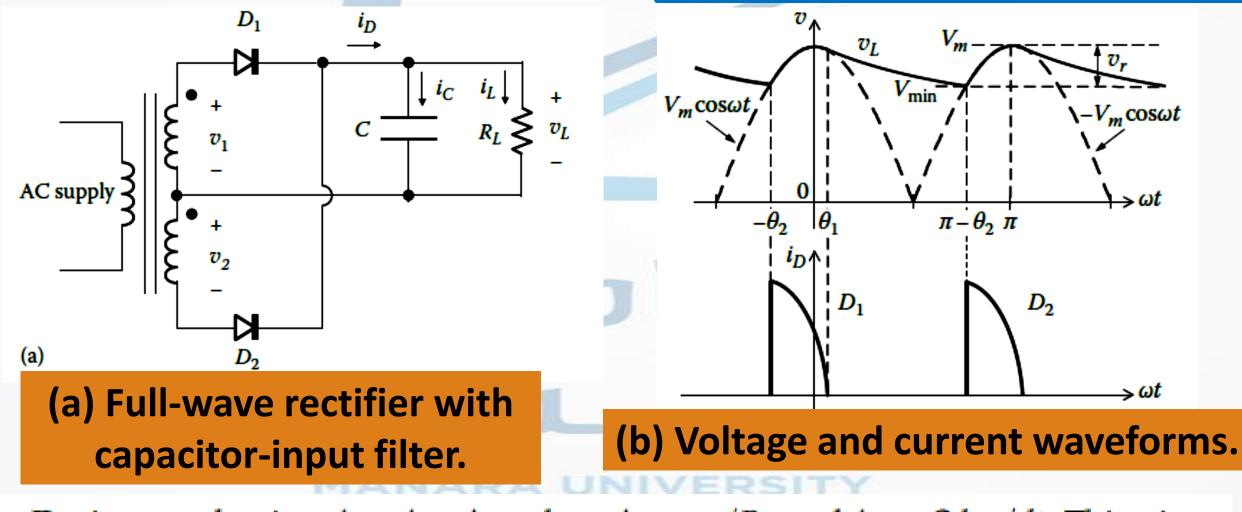


full-wave rectifier circuit with a capacitor-input filter

 $-V_m \cos \omega t$

 $\rightarrow \omega t$

⇒ωt



During conduction, $i_D = i_L + i_C$, where $i_L = v_L/R_L$ and $i_C = Cdv_L/dt$. This gives:

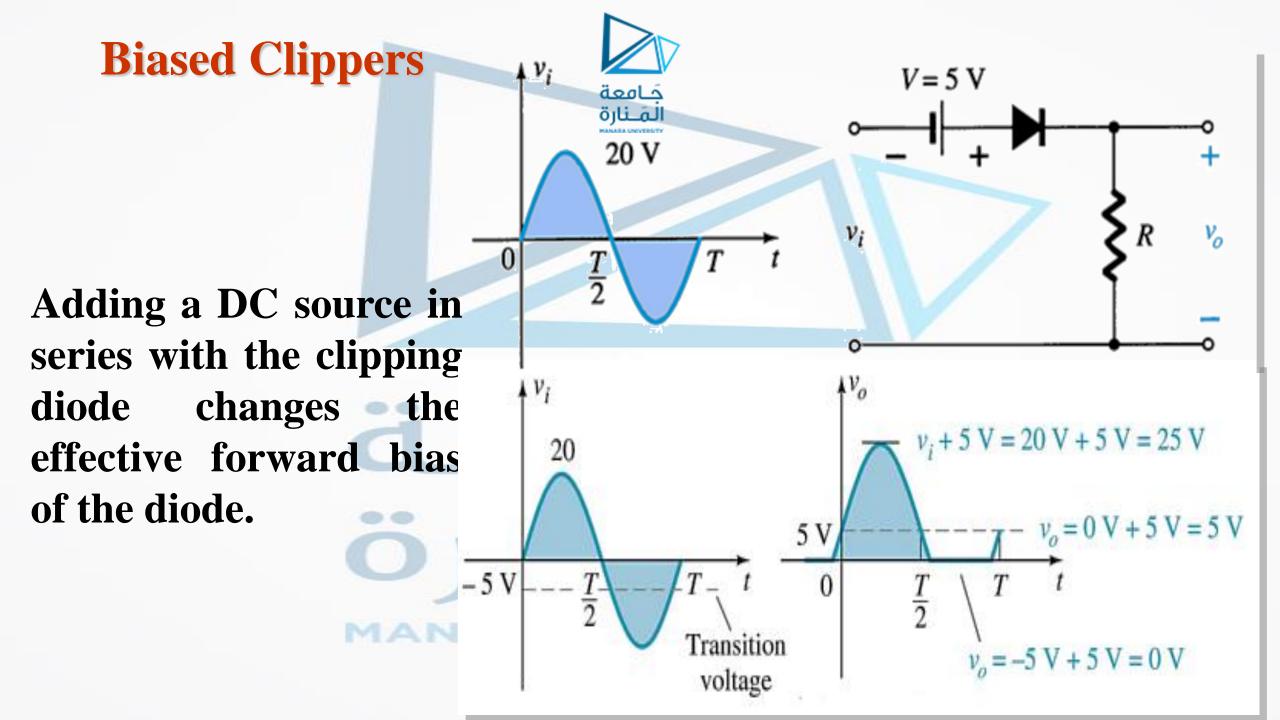


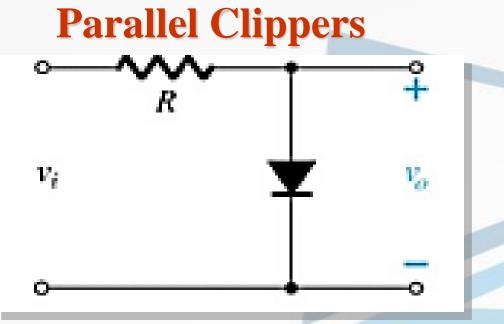
$$i_D = \frac{V_m}{R_L} \cos\omega t - \omega C V_m \sin\omega t, \quad -\theta_2 \le \omega t \le \theta_1$$

- When the diode stops conducting at $\omega t = \theta_1$; iD = 0. $\tan \theta_1 = \frac{1}{2}$
- During the interval $\theta_1 \le \pi \theta_2$, both diodes are nonconducting. C discharges exponentially through R_L , with a time constant R_L C from an initial value $V_m cos \theta_1$ at $\omega t = \theta_1$
- Conduction resumes at $\pi \theta_2$ when the decaying exponential intersects the rising negative half-cycle $v_L = -V_m \cos \theta_1$. Substituting $-V_m \cos \theta_2$

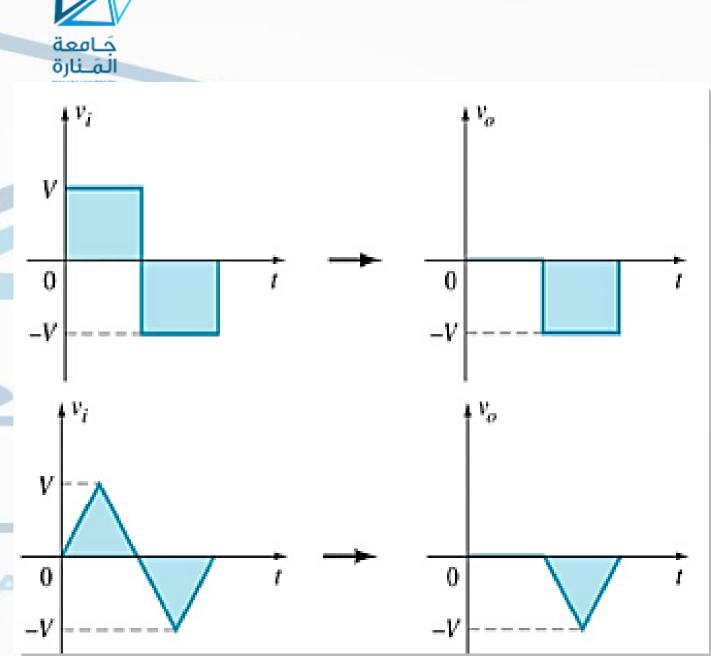
average value of
$$v_L$$
 is:

$$\begin{aligned}
\cos\theta_2 &= \cos\theta_1 e^{-[\pi - (\theta_1 + \theta_2)]/\omega CR_L} \\
V_L &= \frac{V_m}{\pi} \left[\int_{-\theta_2}^{\theta_1} \cos\omega t d(\omega t) + \int_{\theta_1}^{\pi - \theta_2} \cos\theta_1 e^{-(\omega t - \theta_1)/\omega CR_L} d(\omega t) \right]
\end{aligned}$$



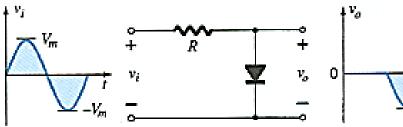


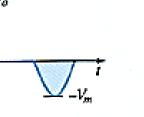
The diode in a parallel clipper circuit "clips" any voltage that forward bias it. DC biasing can be added in series with the diode to change the clipping level.

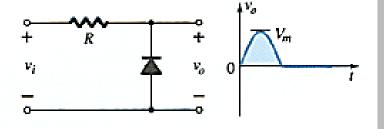


Simple Parallel Clippers (Ideal Diodes)

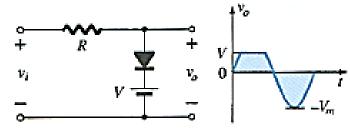
Summary of Clipper Circuits

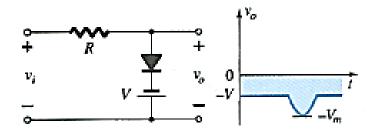


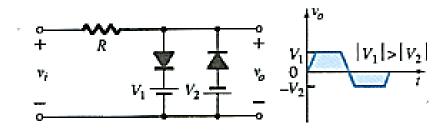


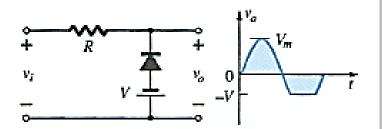


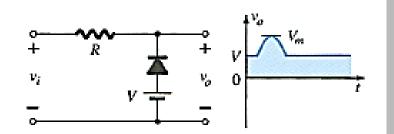
Biased Parallel Clippers (Ideal Diodes)





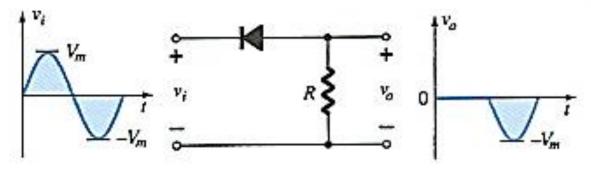






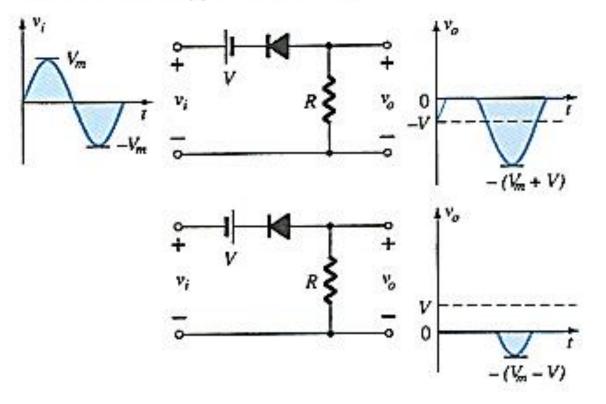
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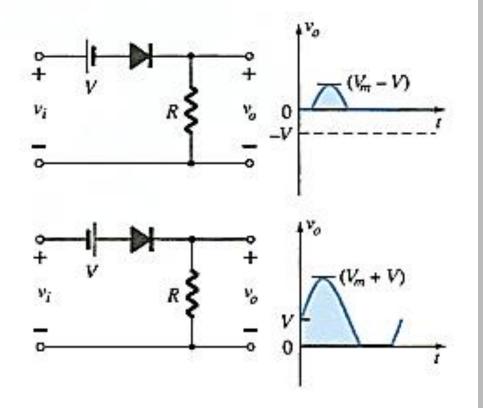
Simple Series Clippers (Ideal Diodes) POSITIVE

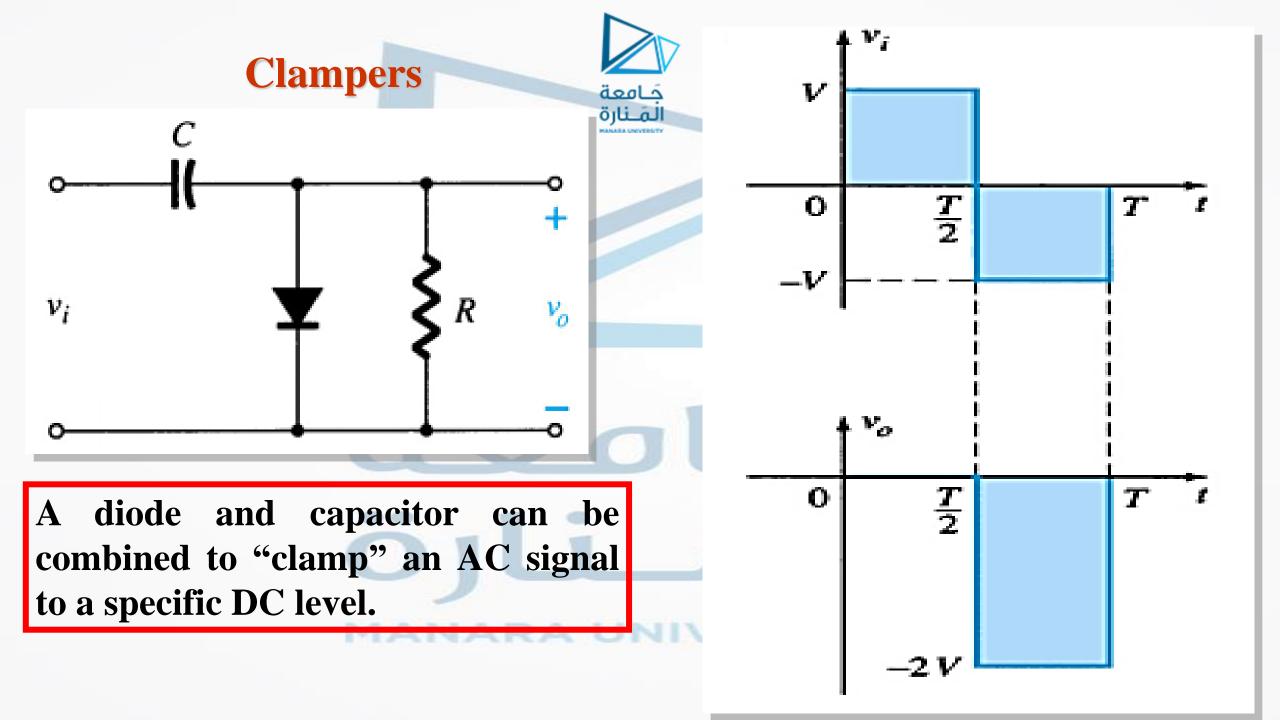


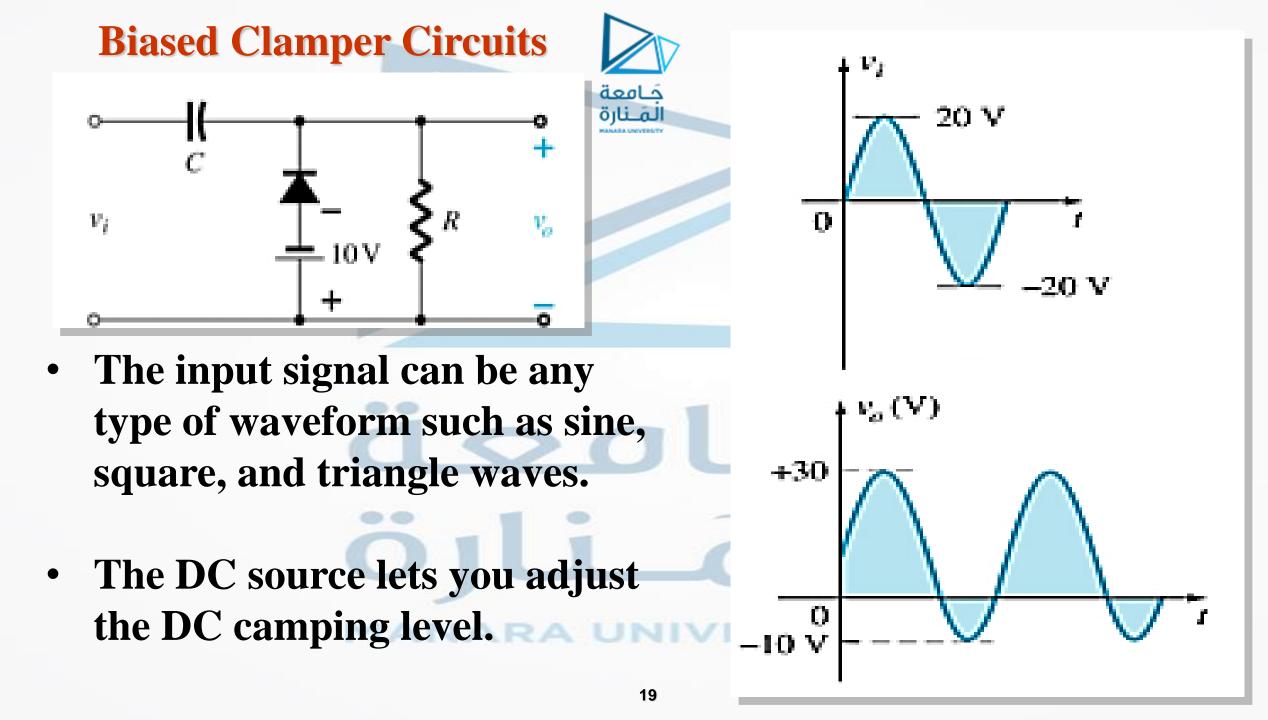
NEGATIVE $\downarrow V_i$ $R \neq V_o$ $\downarrow V_m$

Biased Series Clippers (Ideal Diodes)

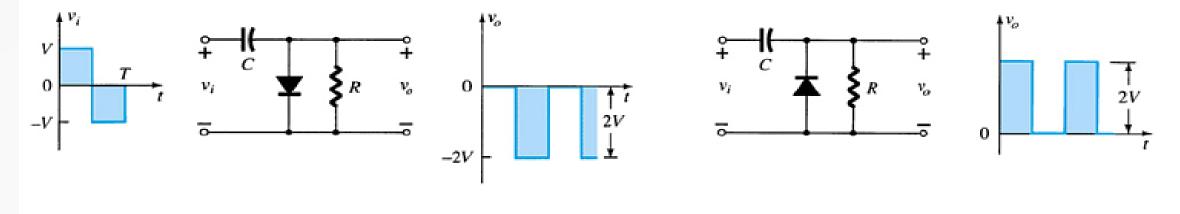


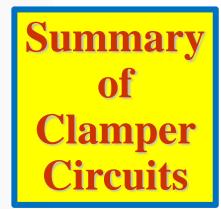


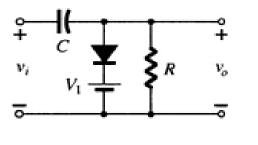


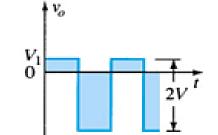


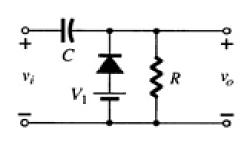
Clamping Networks

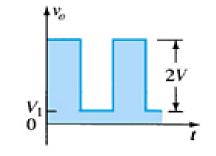


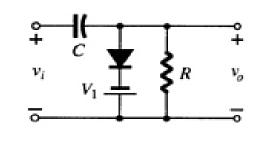


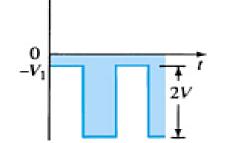




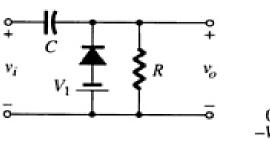


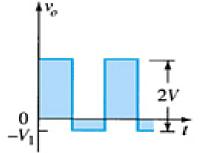


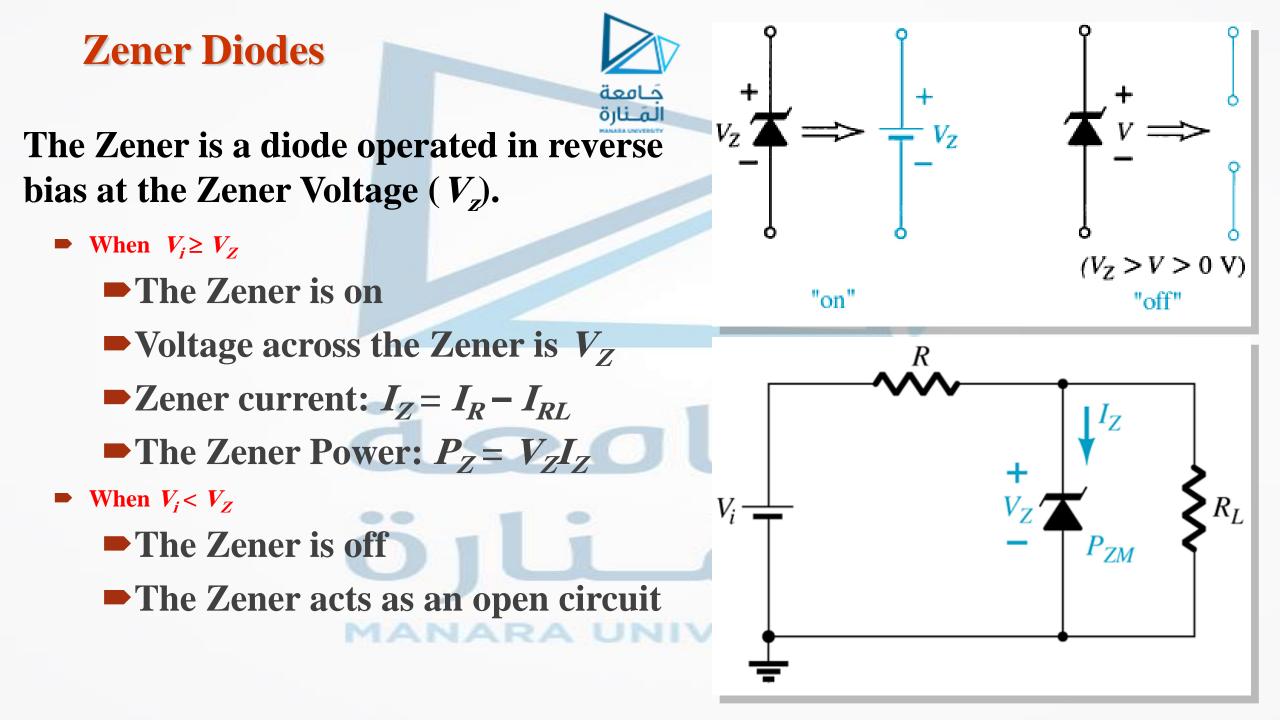




4 Vo







Zener Resistor Values

If R is too large, the Zener diode cannot conduct because the available amount of V_i = current is less than the minimum current rating, I_{ZK}. The minimum current is given by:

$$\boldsymbol{I}_{L\min} = \boldsymbol{I}_{R} - \boldsymbol{I}_{ZK}$$

The maximum value of resistance is:

$$R_{L\max} = \frac{V_Z}{I_{L\min}}$$

If R is too small, the Zener current exceeds the maximum current rating, I_{ZM}. The maximum current for the circuit is given by:

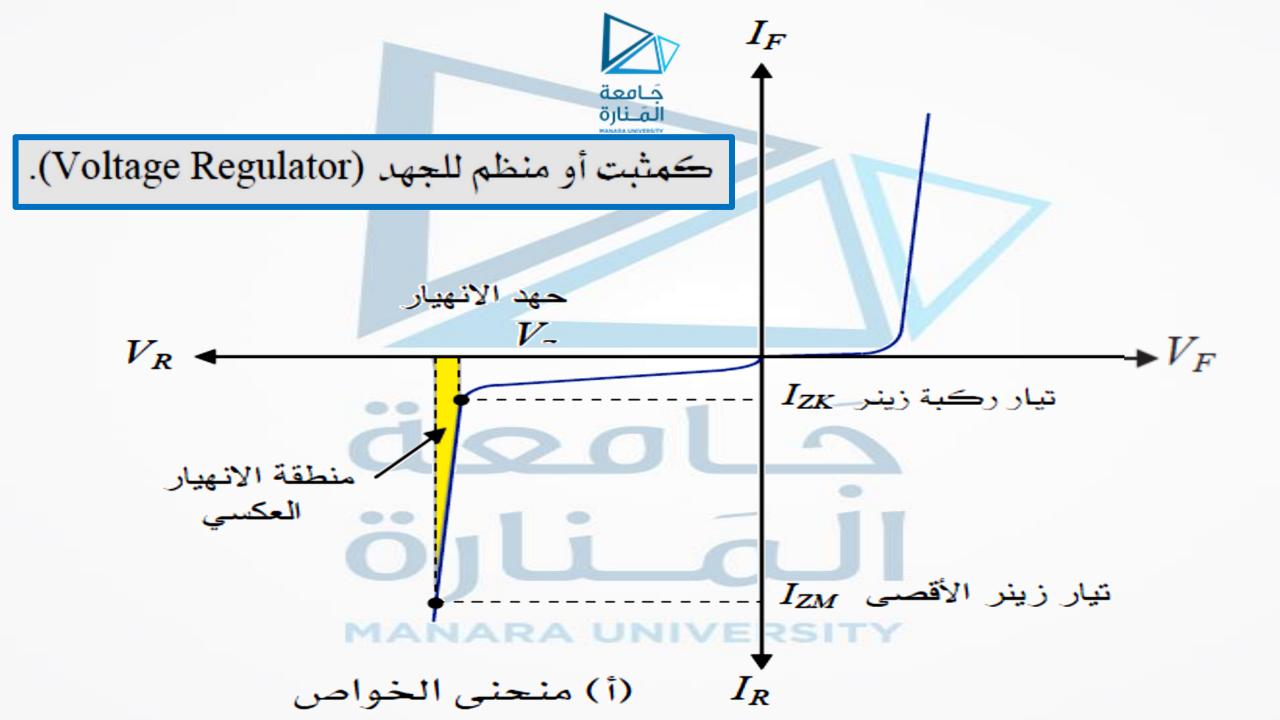
 $I_{L \max} = \frac{V_L}{R_L} = \frac{V_Z}{R_{L \min}}$

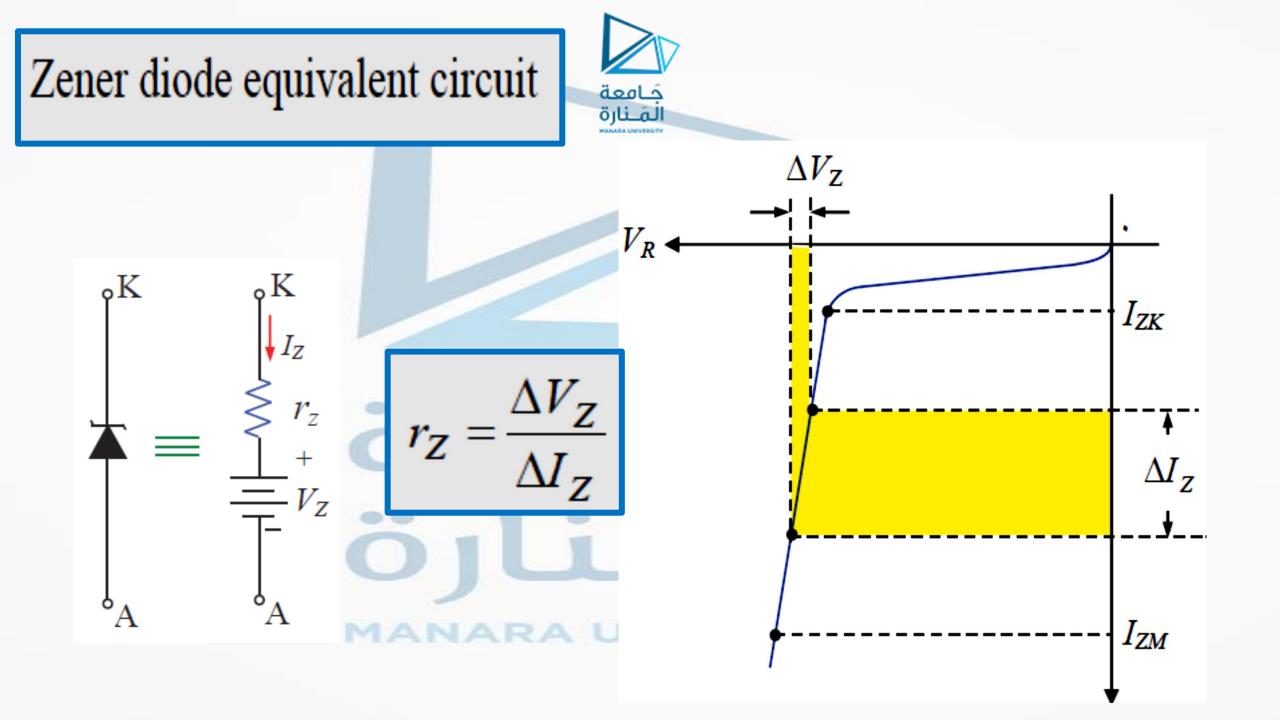
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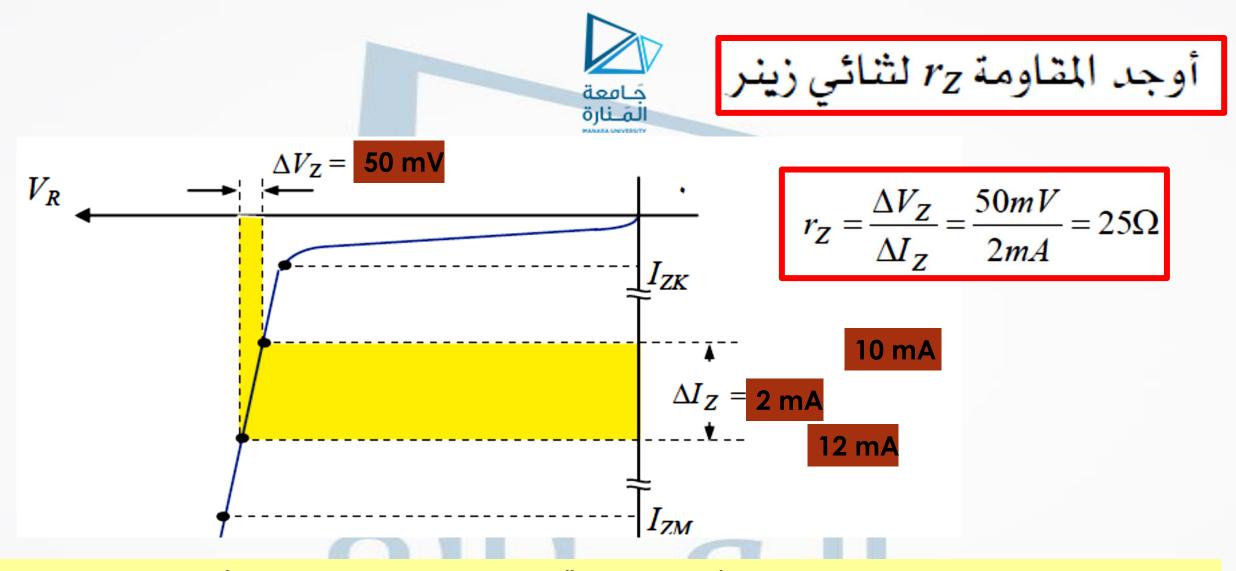
The minimum value of resistance is:

$$R_{L\min} = \frac{RV_Z}{V_i - V_Z}$$

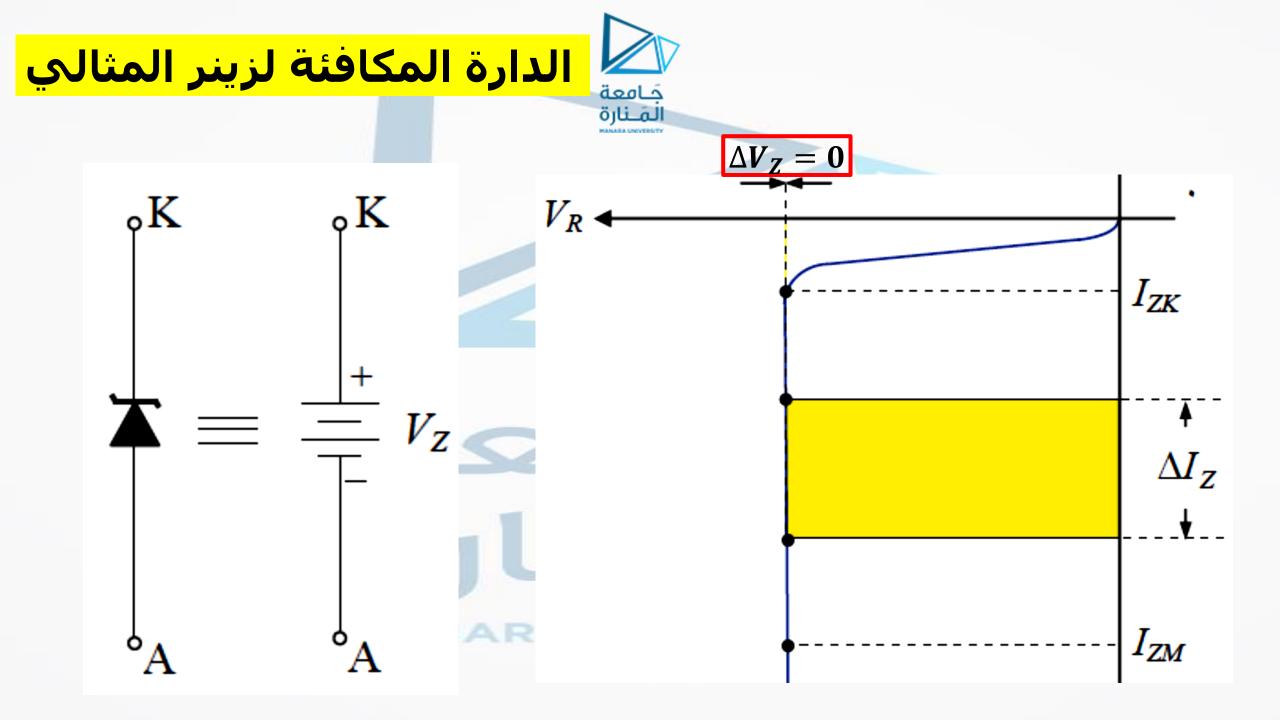
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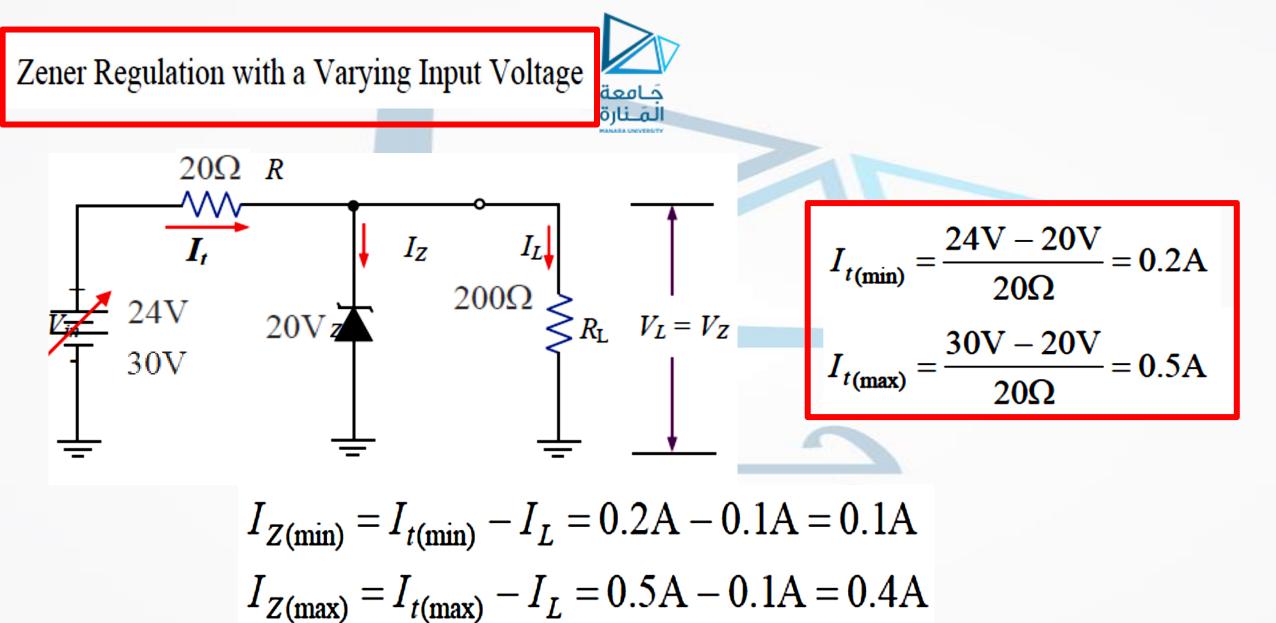




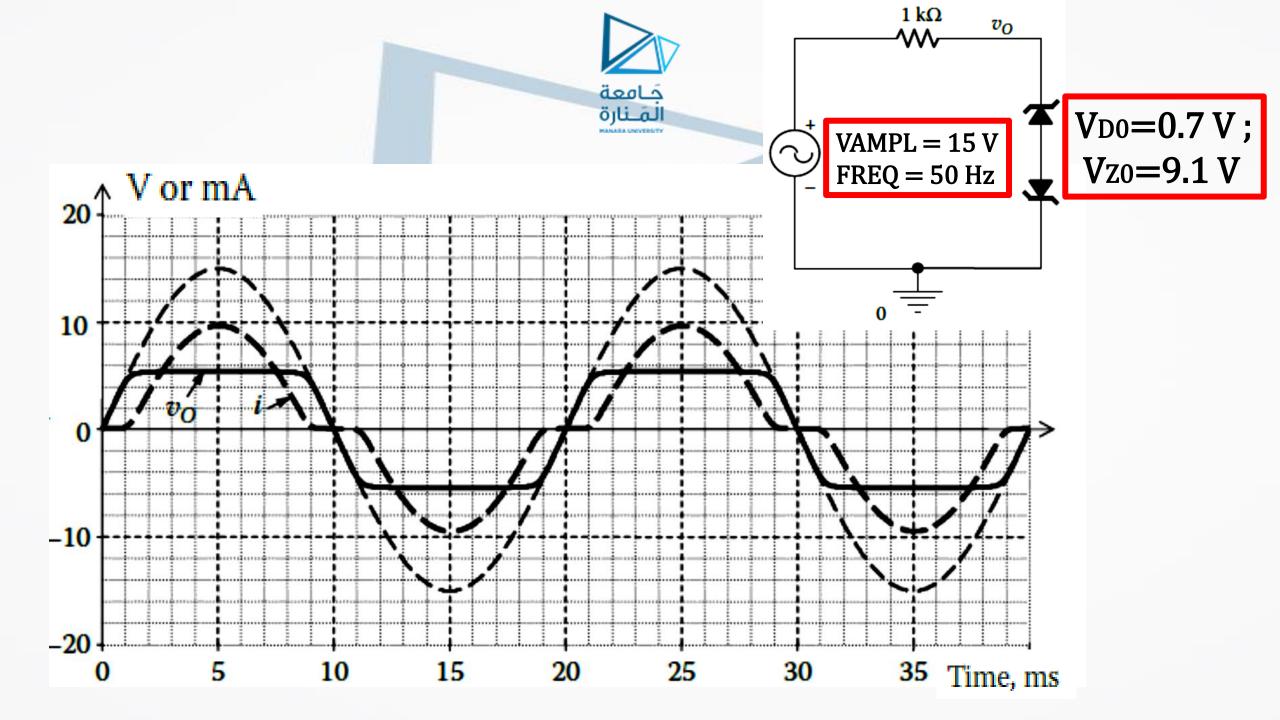


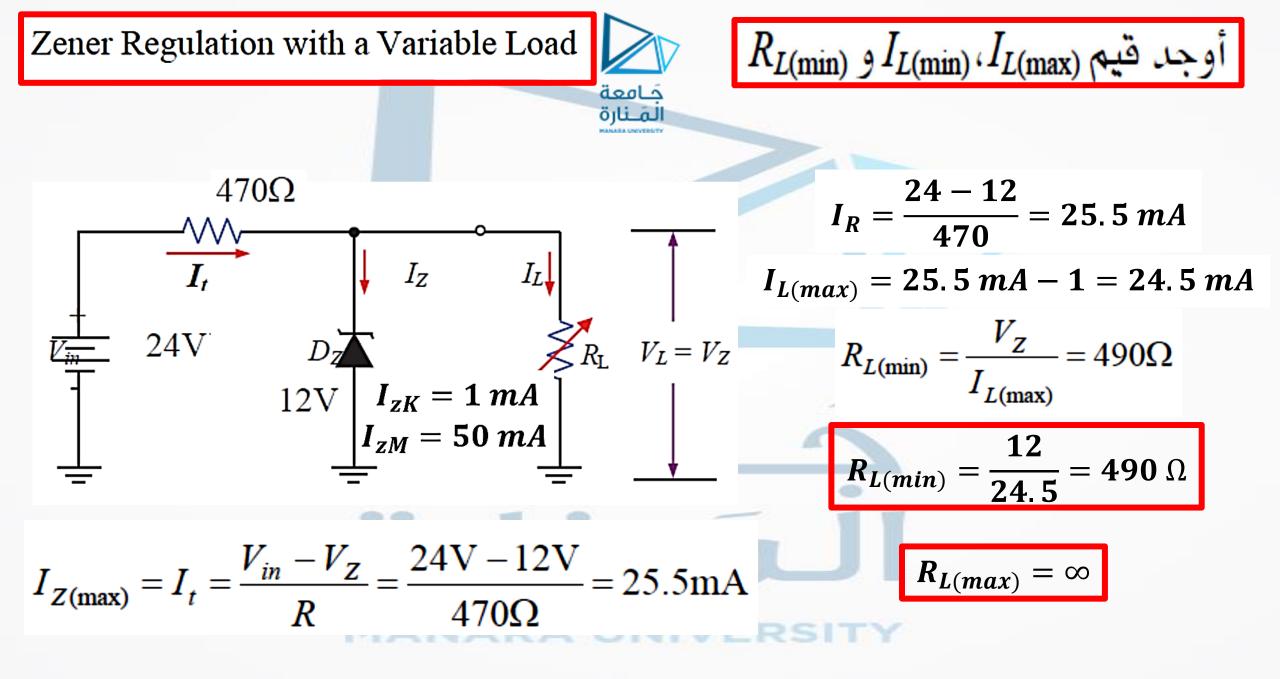
اذا كانت rz=5 Ω و Vz=6.8 Vz فما هي قيمة الجهد على طرفي ثنائي زينر V_{zD} عند مرور تيار مقداره MA. V_{zD} = V_z + I_z rz = 6.8 V+ 20 mA. 5 Ω=6.9 V





 $P_{Z(\text{max})} = V_Z I_{Z(\text{max})} = 0.4\text{A} \ 20\text{V} = 8W$







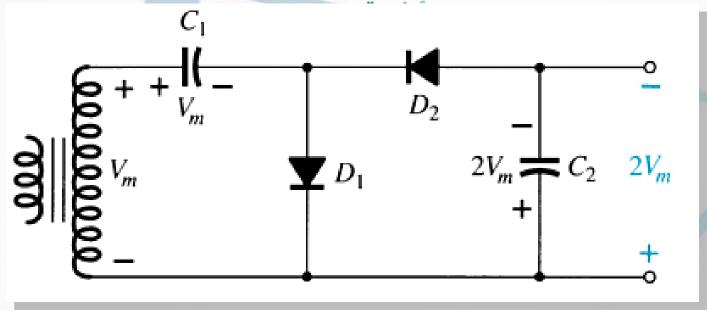
Voltage multiplier circuits use a combination of diodes and

capacitors to step up the output voltage of rectifier circuits.



Voltage Doubler

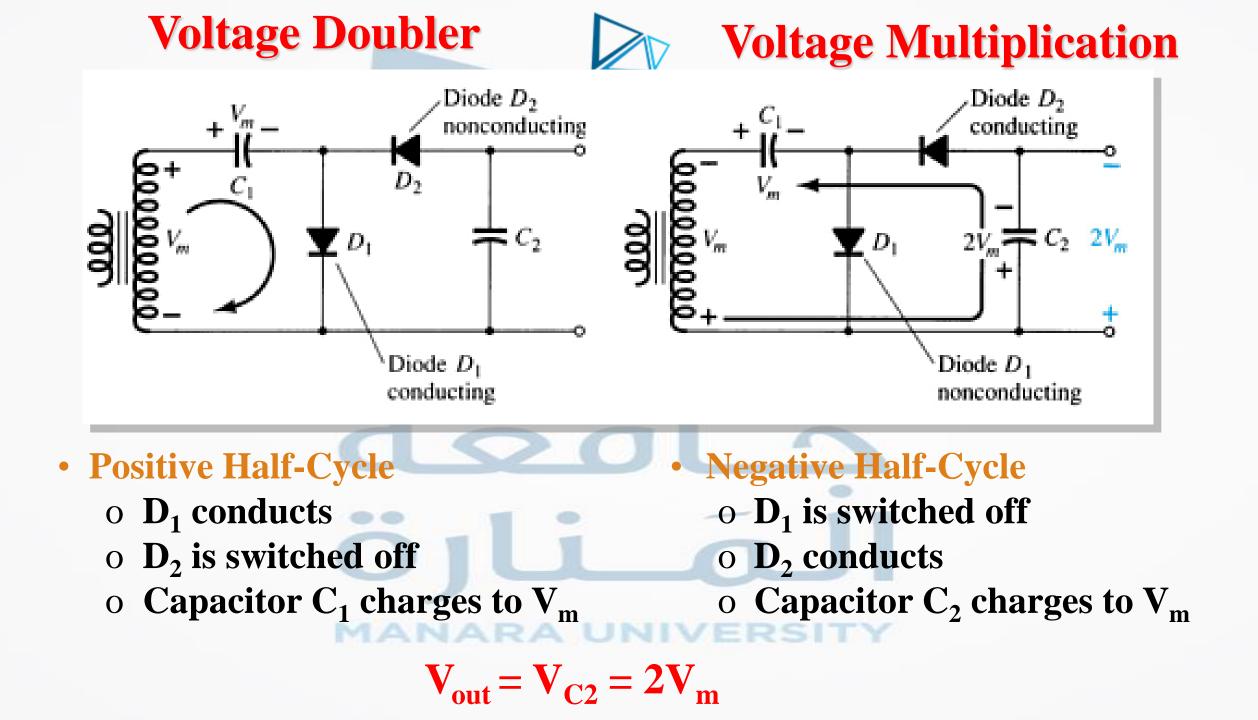




This half-wave voltage doubler's output can be calculated by:

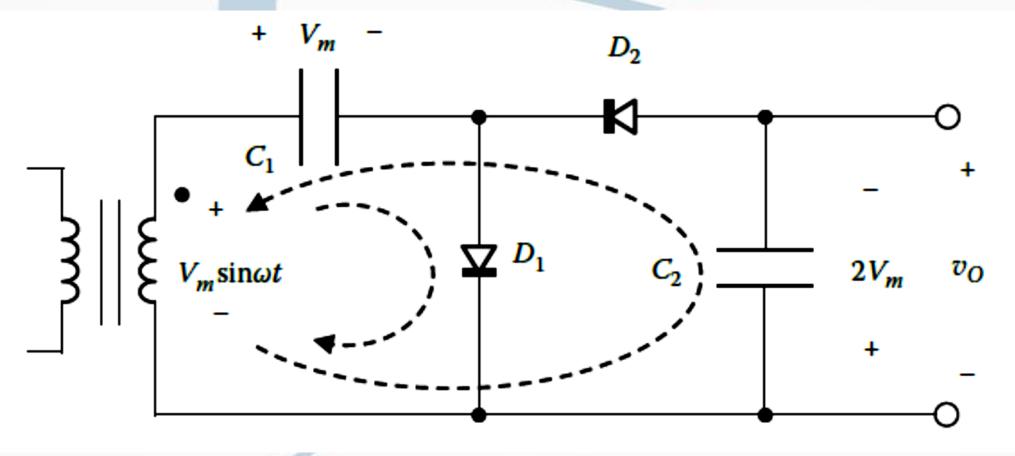
$$\mathbf{V}_{\text{out}} = \mathbf{V}_{\text{C2}} = 2\mathbf{V}_{\text{m}}$$

where V_m = peak secondary voltage of the transformer



Voltage Multiplication





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Voltage Tripler and Quadrupler



