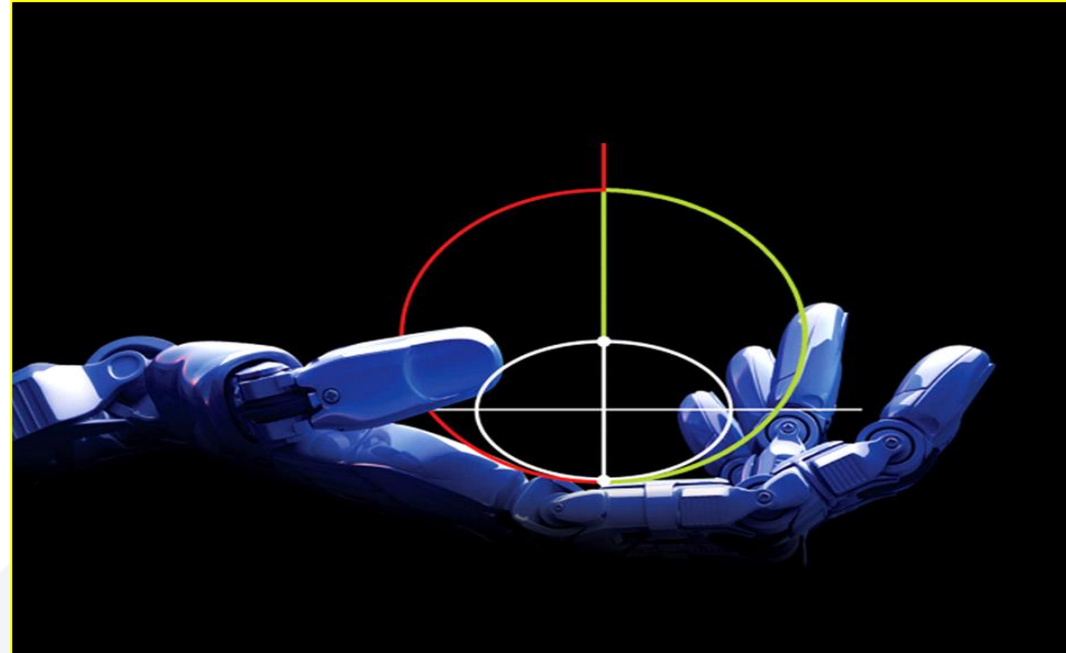


## Planar Kinematics of a Rigid Body Motion Analysis :Acceleration





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**Relative-Motion Analysis : Acceleration**

## Relative-Motion Analysis : Acceleration

An equation that relates the accelerations of two points on a bar (rigid body) subjected to general plane motion may be determined by differentiating  $\mathbf{v}_B = \mathbf{v}_A + \mathbf{v}_{B/A}$  with respect to time. This yields

$$\frac{d\mathbf{v}_B}{dt} = \frac{d\mathbf{v}_A}{dt} + \frac{d\mathbf{v}_{B/A}}{dt}$$

The terms  $d\mathbf{v}_B/dt = \mathbf{a}_B$  and  $d\mathbf{v}_A/dt = \mathbf{a}_A$  represent the *absolute accelerations* of points  $B$  and  $A$ .

The last term represents the acceleration of  $B$  with respect to  $A$  as measured by an observer fixed to translating  $x'$ ,  $y'$  axes which have their origin at the base point  $A$ . It was shown that to this observer point  $B$  appears to move along a *circular arc* that has a radius of curvature

$r_{B/A}$ . Consequently,  $\mathbf{a}_{B/A}$  can be expressed in terms of its tangential and normal components; i.e.,  $\mathbf{a}_{B/A} = (\mathbf{a}_{B/A})_t + (\mathbf{a}_{B/A})_n$ , where  $(a_{B/A})_t = \alpha r_{B/A}$  and  $(a_{B/A})_n = \omega^2 r_{B/A}$ . Hence, the relative-acceleration equation can be written in the form

$$\mathbf{a}_B = \mathbf{a}_A + (\mathbf{a}_{B/A})_t + (\mathbf{a}_{B/A})_n$$

where

$\mathbf{a}_B$  = acceleration of point  $B$

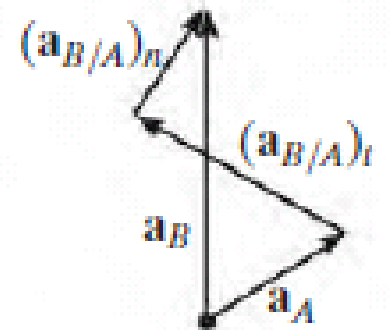
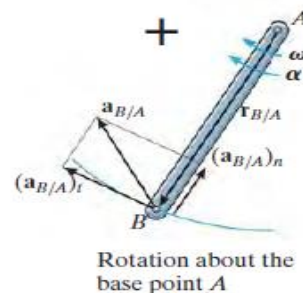
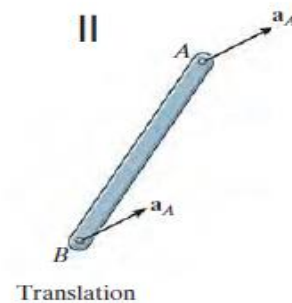
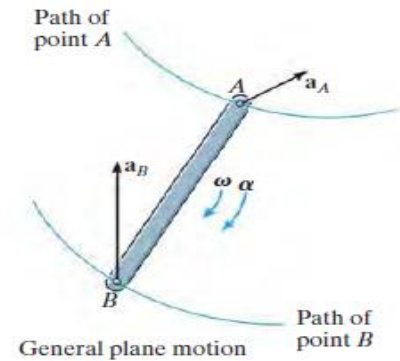
$\mathbf{a}_A$  = acceleration of point  $A$

$(\mathbf{a}_{B/A})_t$  = tangential acceleration component of  $B$  with respect to  $A$ . The *magnitude* is  $(a_{B/A})_t = \alpha r_{B/A}$ , and the *direction* is perpendicular to  $\mathbf{r}_{B/A}$ .

$(\mathbf{a}_{B/A})_n$  = normal acceleration component of  $B$  with respect to  $A$ . The *magnitude* is  $(a_{B/A})_n = \omega^2 r_{B/A}$ , and the *direction* is always from  $B$  toward  $A$ .

It is seen that at a given instant the acceleration of  $B$  is determined by considering the bar to translate with an acceleration  $\mathbf{a}_A$ , and simultaneously rotate about the base point  $A$  with an instantaneous angular velocity  $\omega$  and angular acceleration  $\alpha$ .

Vector addition of these two effects, applied to  $B$ , yields  $\mathbf{a}_B$ . It should be noted that since points  $A$  and  $B$  move along curved paths, the accelerations of these points will have both tangential and normal components.



Since the relative-acceleration components represent the effect of *circular motion* observed from translating axes having their origin at the base point  $A$ , these terms can be expressed as  $(\mathbf{a}_{B/A})_t = \boldsymbol{\alpha} \times \mathbf{r}_{B/A}$  and  $(\mathbf{a}_{B/A})_n = -\omega^2 \mathbf{r}_{B/A}$

$$\mathbf{a}_B = \mathbf{a}_A + \boldsymbol{\alpha} \times \mathbf{r}_{B/A} - \omega^2 \mathbf{r}_{B/A}$$

where

$\mathbf{a}_B$  = acceleration of point  $B$

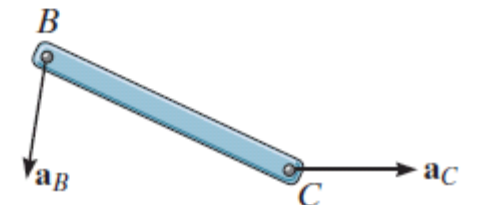
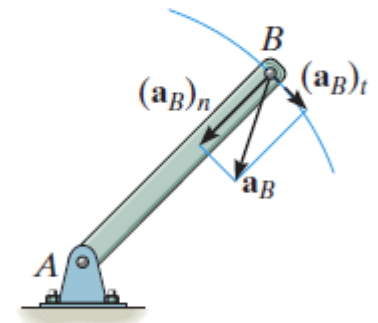
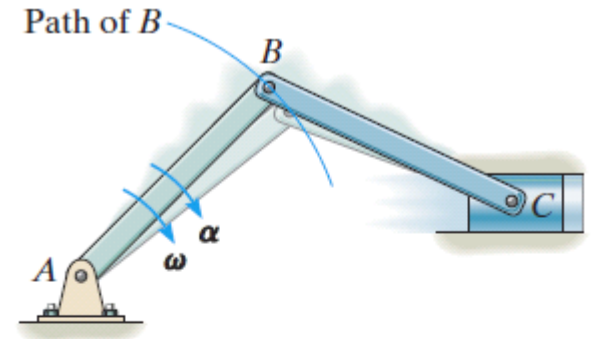
$\mathbf{a}_A$  = acceleration of the base point  $A$

$\boldsymbol{\alpha}$  = angular acceleration of the body

$\boldsymbol{\omega}$  = angular velocity of the body

$\mathbf{r}_{B/A}$  = position vector directed from  $A$  to  $B$

If equations are applied in a practical manner to study the accelerated motion of a rigid body which is *pin connected to two other bodies*, it should be realized that points which are *coincident at the pin* move with the *same acceleration*, since the *path of motion over which they travel is the same*. For example, point **B** lying on either rod **BA** or **BC** of the crank mechanism shown has the same acceleration, since the rods are pin connected at **B**. Here the motion of **B** is along a *circular path*, so that  **$a_B$**  can be expressed in terms of its tangential and normal components. At the other end of rod **BC** point **C** moves along a *straight-lined path*, which is defined by the piston. Hence,  **$a_C$**  is *horizontal*



Finally, consider a disk that rolls without slipping as shown. As a result,  $v_A = 0$  and so from the kinematic diagram, the velocity of the mass center  $G$  is

$$\mathbf{v}_G = \mathbf{v}_A + \boldsymbol{\omega} \times \mathbf{r}_{G/A} = \mathbf{0} + (-\omega \mathbf{k}) \times (r \mathbf{j})$$

So that

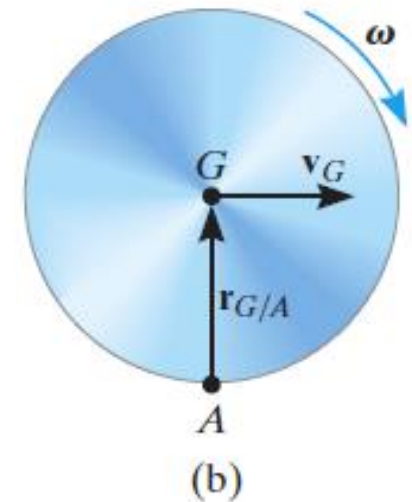
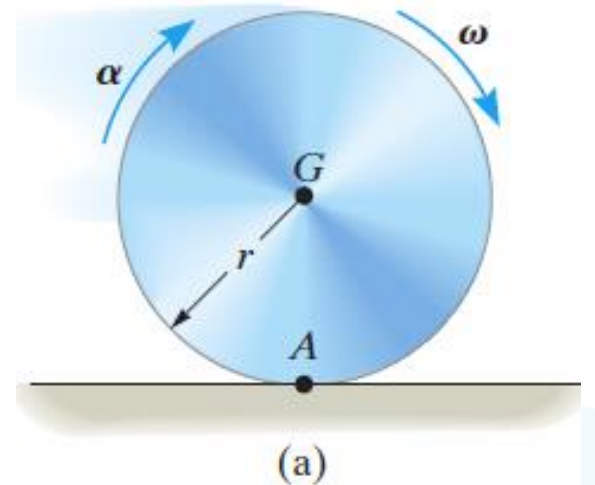
$$v_G = \omega r$$

This same result can also be determined using the IC method where point  $A$  is the *IC*.

Since  $G$  moves along a *straight line*, its acceleration in this case can be determined from the time derivative of its velocity.

$$\frac{dv_G}{dt} = \frac{d\omega}{dt} r$$

$$a_G = \alpha r$$





## Procedure for Analysis

The relative acceleration equation can be applied between any two points  $A$  and  $B$  on a body either by using a Cartesian vector analysis, or by writing the  $x$  and  $y$  scalar component equations directly.

### Velocity Analysis.

- Determine the angular velocity  $\omega$  of the body by using a velocity analysis . Also, determine velocities  $v_A$  and  $v_B$  of points  $A$  and  $B$  if these points move along curved paths.

## Vector Analysis

### Kinematic Diagram.

- Establish the directions of the fixed  $x, y$  coordinates and draw the kinematic diagram of the body. Indicate on it  $\mathbf{a}_A, \mathbf{a}_B, \boldsymbol{\omega}, \boldsymbol{\alpha}$ , and  $\mathbf{r}_{B/A}$ .
- If points  $A$  and  $B$  move along *curved paths*, then their accelerations should be indicated in terms of their tangential and normal components, i.e.,  $\mathbf{a}_A = (\mathbf{a}_A)_t + (\mathbf{a}_A)_n$  and  $\mathbf{a}_B = (\mathbf{a}_B)_t + (\mathbf{a}_B)_n$ .

### Acceleration Equation.

- To apply  $\mathbf{a}_B = \mathbf{a}_A + \boldsymbol{\alpha} \times \mathbf{r}_{B/A} - \omega^2 \mathbf{r}_{B/A}$ , express the vectors in Cartesian vector form and substitute them into the equation. Evaluate the cross product and then equate the respective  $\mathbf{i}$  and  $\mathbf{j}$  components to obtain two scalar equations.
- If the solution yields a *negative* answer for an *unknown* magnitude, it indicates that the sense of direction of the vector is opposite to that shown on the kinematic diagram.

## Scalar Analysis Kinematic Diagram.

- If the acceleration equation is applied in scalar form, then the magnitudes and directions of the relative-acceleration components  $(\mathbf{a}_{B/A})_t$  and  $(\mathbf{a}_{B/A})_n$  must be established. To do this draw a kinematic diagram such as shown. Since the body is considered to be momentarily “pinned” at the base point  $A$ , the *magnitudes* of these components are  $(a_{B/A})_t = \alpha r_{B/A}$  and  $(a_{B/A})_n = \omega^2 r_{B/A}$ . Their *sense of direction* is established from the diagram such that  $(\mathbf{a}_{B/A})_t$  acts perpendicular to  $\mathbf{r}_{B/A}$ , in accordance with the rotational motion  $\alpha$  of the body, and  $(\mathbf{a}_{B/A})_n$  is directed from  $B$  toward  $A$ .

## Acceleration Equation.

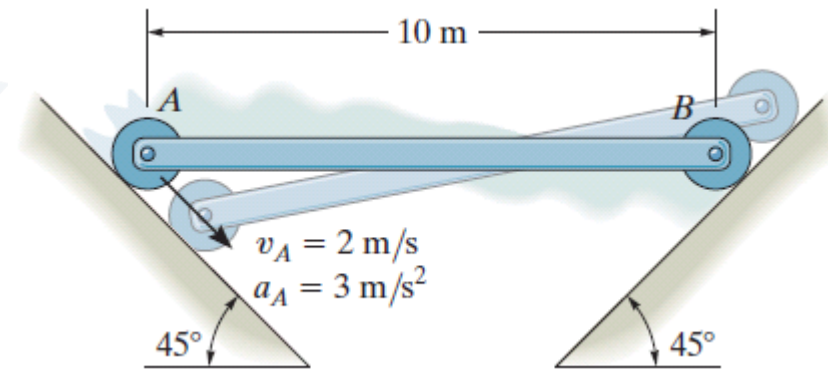
- Represent the vectors in  $\mathbf{a}_B = \mathbf{a}_A + (\mathbf{a}_{B/A})_t + (\mathbf{a}_{B/A})_n$  graphically by showing their magnitudes and directions underneath each term. The scalar equations are determined from the  $x$  and  $y$  components of these vectors.

## EXAMPLE

The rod  $AB$  shown is confined to move along the inclined planes at  $A$  and  $B$ . If point  $A$  has an acceleration of  $3 \text{ m/s}^2$  and a velocity of  $2 \text{ m/s}$ , both directed down the plane at the instant the rod is horizontal, determine the angular acceleration of the rod at this instant.

### SOLUTION I (VECTOR ANALYSIS)

We will apply the acceleration equation to points  $A$  and  $B$  on the rod. To do so it is first necessary to determine the angular velocity of the rod. Show that it is  $\omega = 0.283 \text{ rad/s}$  using either the velocity equation or the method of instantaneous centers.



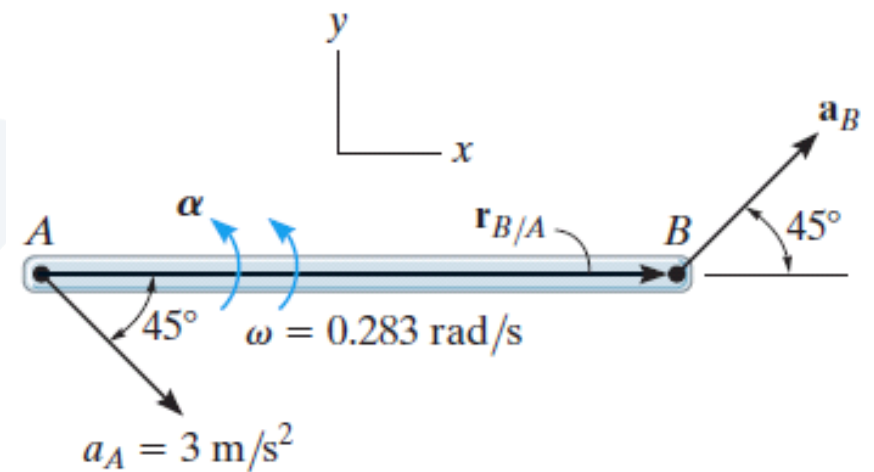
**Kinematic Diagram.** Since points  $A$  and  $B$  both move along straight-line paths, they have *no* components of acceleration normal to the paths. There are two unknowns, namely,  $a_B$  and  $\alpha$ .

**Acceleration Equation.**

$$\mathbf{a}_B = \mathbf{a}_A + \boldsymbol{\alpha} \times \mathbf{r}_{B/A} - \omega^2 \mathbf{r}_{B/A}$$

$$a_B \cos 45^\circ \mathbf{i} + a_B \sin 45^\circ \mathbf{j} = 3 \cos 45^\circ \mathbf{i} - 3 \sin 45^\circ \mathbf{j} + (\alpha \mathbf{k}) \times (10 \mathbf{i}) - (0.283)^2 (10 \mathbf{i})$$

Carrying out the cross product and equating the  $\mathbf{i}$  and  $\mathbf{j}$  components yields



$$a_B \cos 45^\circ = 3 \cos 45^\circ - (0.283)^2(10) \quad (1)$$

$$a_B \sin 45^\circ = -3 \sin 45^\circ + \alpha(10) \quad (2)$$

Solving, we have

$$a_B = 1.87 \text{ m/s}^2 \nearrow 45^\circ$$

$$\alpha = 0.344 \text{ rad/s}^2 \curvearrowright$$

*Ans.*

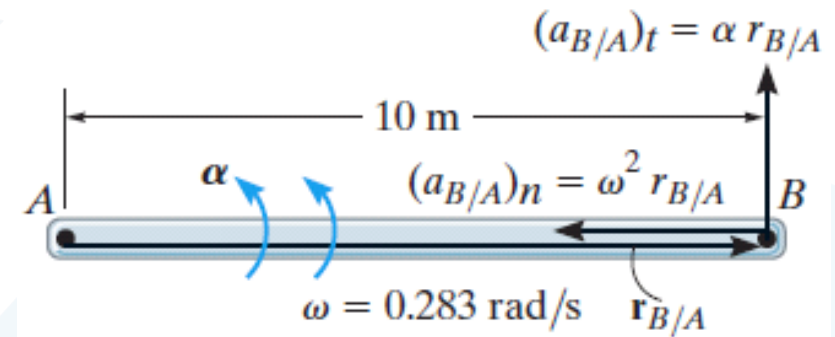
## SOLUTION II (SCALAR ANALYSIS)

From the kinematic diagram, showing the relative-acceleration components  $(\mathbf{a}_{B/A})_t$  and  $(\mathbf{a}_{B/A})_n$ , we have

$$\mathbf{a}_B = \mathbf{a}_A + (\mathbf{a}_{B/A})_t + (\mathbf{a}_{B/A})_n$$

$$\begin{bmatrix} a_B \\ \nearrow 45^\circ \end{bmatrix} = \begin{bmatrix} 3 \text{ m/s}^2 \\ \searrow 45^\circ \end{bmatrix} + \begin{bmatrix} \alpha(10 \text{ m}) \\ \uparrow \end{bmatrix} + \begin{bmatrix} (0.283 \text{ rad/s})^2(10 \text{ m}) \\ \leftarrow \end{bmatrix}$$

Equating the  $x$  and  $y$  components yields Eqs. 1 and 2, and the solution proceeds as before.



## EXAMPLE

The disk rolls without slipping and has the angular motion shown. Determine the acceleration of point  $A$  at this instant.

### SOLUTION I (VECTOR ANALYSIS)

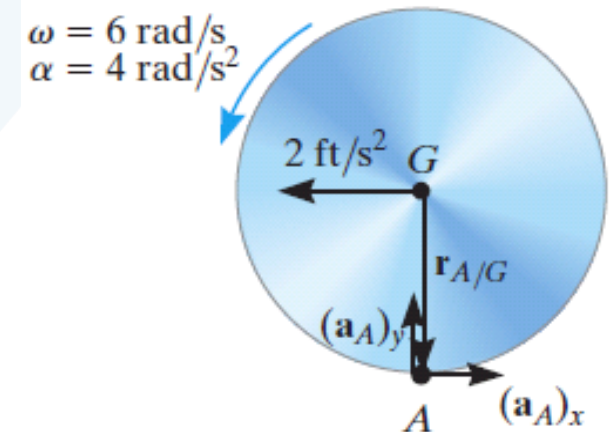
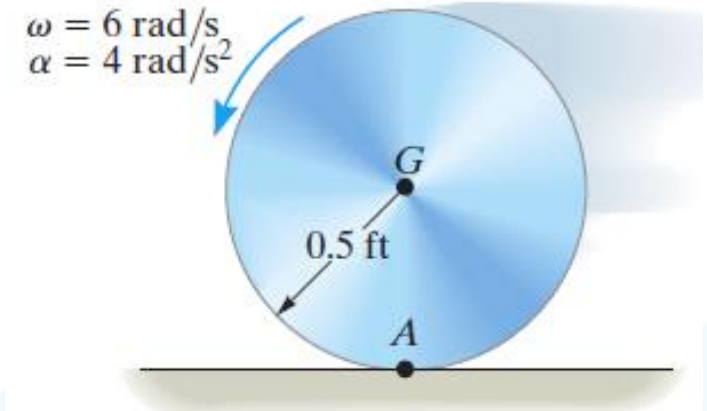
**Kinematic Diagram.** Since no slipping occurs,

$$a_G = \alpha r = (4 \text{ rad/s}^2)(0.5 \text{ ft}) = 2 \text{ ft/s}^2$$

### Acceleration Equation.

We will apply the acceleration equation to points  $G$  and  $A$

$$\begin{aligned} \mathbf{a}_A &= \mathbf{a}_G + \boldsymbol{\alpha} \times \mathbf{r}_{A/G} - \omega^2 \mathbf{r}_{A/G} \\ \mathbf{a}_A &= -2\mathbf{i} + (4\mathbf{k}) \times (-0.5\mathbf{j}) - (6)^2(-0.5\mathbf{j}) \\ &= \{18\mathbf{j}\} \text{ ft/s}^2 \end{aligned}$$





## SOLUTION II (SCALAR ANALYSIS)

Using the result for  $a_G = 2 \text{ ft/s}^2$  determined above, and from the kinematic diagram, showing the relative motion  $\mathbf{a}_{A/G}$ , we have

$$\mathbf{a}_A = \mathbf{a}_G + (\mathbf{a}_{A/G})_x + (\mathbf{a}_{A/G})_y$$

$$\begin{bmatrix} (a_A)_x \\ \rightarrow \end{bmatrix} + \begin{bmatrix} (a_A)_y \\ \uparrow \end{bmatrix} = \begin{bmatrix} 2 \text{ ft/s}^2 \\ \leftarrow \end{bmatrix} + \begin{bmatrix} (4 \text{ rad/s}^2)(0.5 \text{ ft}) \\ \rightarrow \end{bmatrix} + \begin{bmatrix} (6 \text{ rad/s})^2(0.5 \text{ ft}) \\ \uparrow \end{bmatrix}$$

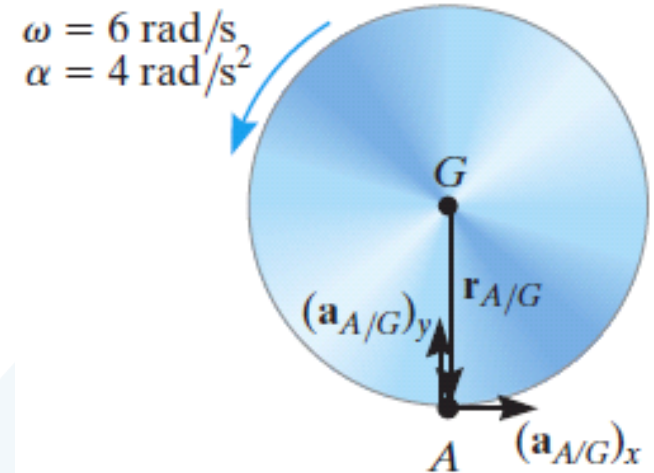
$$\xrightarrow{+} \quad (a_A)_x = -2 + 2 = 0$$

$$+\uparrow \quad (a_A)_y = 18 \text{ ft/s}^2$$

Therefore,

$$a_A = \sqrt{(0)^2 + (18 \text{ ft/s}^2)^2} = 18 \text{ ft/s}^2$$

*Ans.*



## EXAMPLE

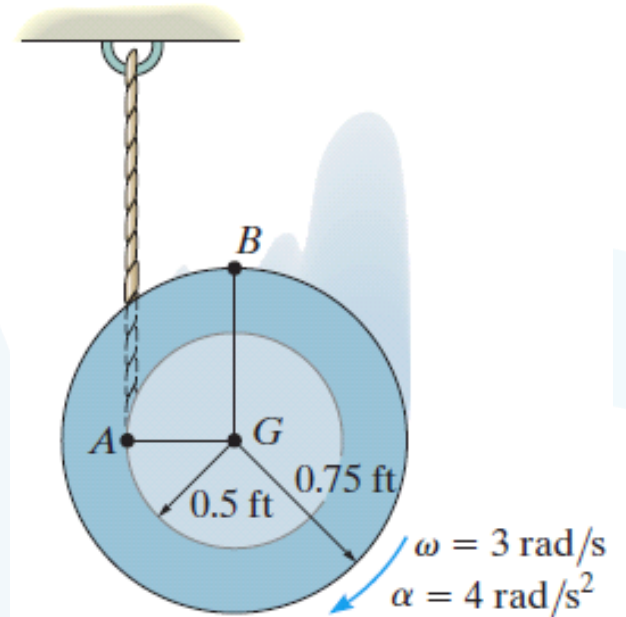
The spool shown unravels from the cord, such that at the instant shown it has an angular velocity of  $3 \text{ rad/s}$  and an angular acceleration of  $4 \text{ rad/s}^2$ . Determine the acceleration of point  $B$ .

### SOLUTION I (VECTOR ANALYSIS)

The spool “appears” to be rolling downward without slipping at point  $A$ . Therefore, we can determine the acceleration of point  $G$

$$a_G = \alpha r = (4 \text{ rad/s}^2)(0.5 \text{ ft}) = 2 \text{ ft/s}^2$$

We will apply the acceleration equation to points  $G$  and  $B$ .



**Kinematic Diagram.** Point  $B$  moves along a *curved path* having an *unknown* radius of curvature. Its acceleration will be represented by its unknown  $x$  and  $y$  components as shown

**Acceleration Equation.**

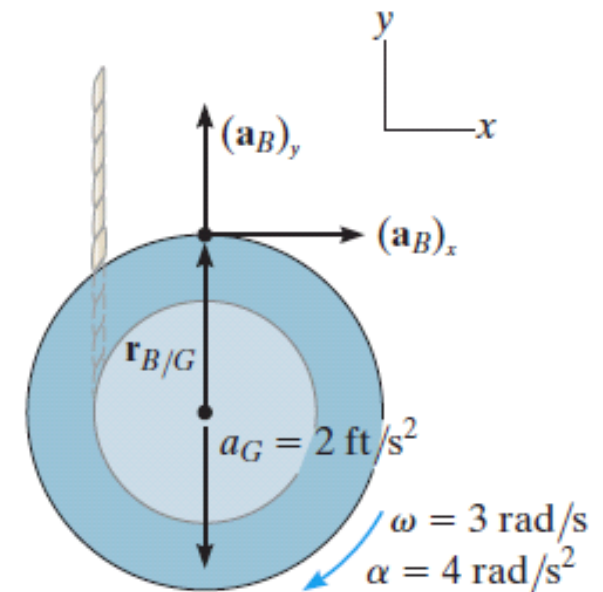
$$\mathbf{a}_B = \mathbf{a}_G + \boldsymbol{\alpha} \times \mathbf{r}_{B/G} - \omega^2 \mathbf{r}_{B/G}$$

$$(a_B)_x \mathbf{i} + (a_B)_y \mathbf{j} = -2\mathbf{j} + (-4\mathbf{k}) \times (0.75\mathbf{j}) - (3)^2(0.75\mathbf{j})$$

Equating the  $\mathbf{i}$  and  $\mathbf{j}$  terms, the component equations are

$$(a_B)_x = 4(0.75) = 3 \text{ ft/s}^2 \rightarrow \quad (1)$$

$$(a_B)_y = -2 - 6.75 = -8.75 \text{ ft/s}^2 = 8.75 \text{ ft/s}^2 \downarrow \quad (2)$$



The magnitude and direction of  $\mathbf{a}_B$  are therefore

$$a_B = \sqrt{(3)^2 + (8.75)^2} = 9.25 \text{ ft/s}^2$$

*Ans.*

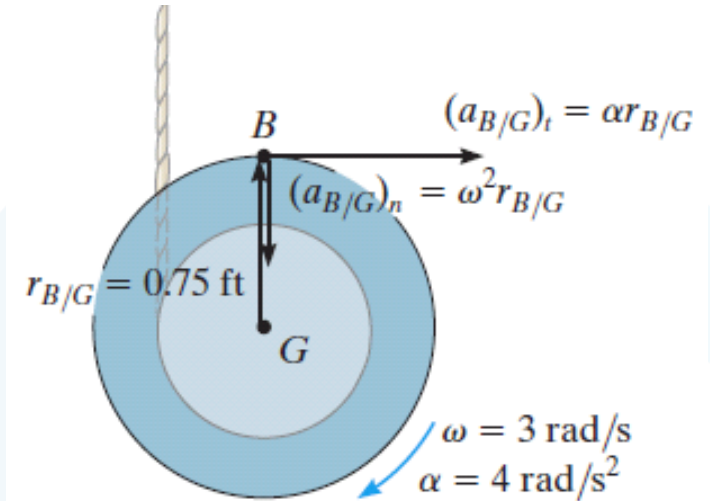
$$\theta = \tan^{-1} \frac{8.75}{3} = 71.1^\circ \swarrow$$

*Ans.*

### SOLUTION II (SCALAR ANALYSIS)

This problem may be solved by writing the scalar component equations directly. The kinematic diagram shows the relative-acceleration components  $(\mathbf{a}_{B/G})_t$  and  $(\mathbf{a}_{B/G})_n$ . Thus,

$$\mathbf{a}_B = \mathbf{a}_G + (\mathbf{a}_{B/G})_t + (\mathbf{a}_{B/G})_n$$



$$\begin{aligned} \begin{bmatrix} (a_B)_x \\ \rightarrow \end{bmatrix} + \begin{bmatrix} (a_B)_y \\ \uparrow \end{bmatrix} \\ = \begin{bmatrix} 2 \text{ ft/s}^2 \\ \downarrow \end{bmatrix} + \begin{bmatrix} 4 \text{ rad/s}^2 (0.75 \text{ ft}) \\ \rightarrow \end{bmatrix} + \begin{bmatrix} (3 \text{ rad/s})^2 (0.75 \text{ ft}) \\ \downarrow \end{bmatrix} \end{aligned}$$

The  $x$  and  $y$  components yield Eqs. 1 and 2 above.

## EXAMPLE

The collar  $C$  moves downward with an acceleration of  $1 \text{ m/s}^2$ . At the instant shown, it has a speed of  $2 \text{ m/s}$  which gives links  $CB$  and  $AB$  an angular velocity  $\omega_{AB} = \omega_{CB} = 10 \text{ rad/s}$ . Determine the angular accelerations of  $CB$  and  $AB$  at this instant.

## SOLUTION (VECTOR ANALYSIS)

**Kinematic Diagram.** The kinematic diagrams of *both* links  $AB$  and  $CB$  are shown. To solve, we will apply the appropriate kinematic equation to each link.

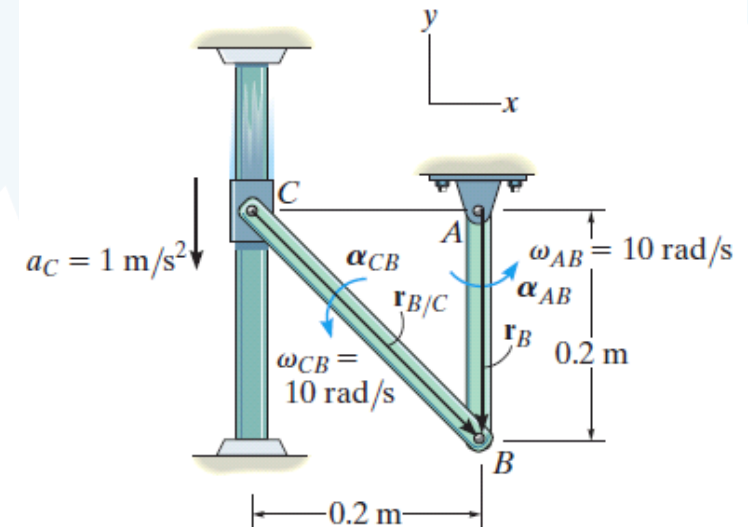
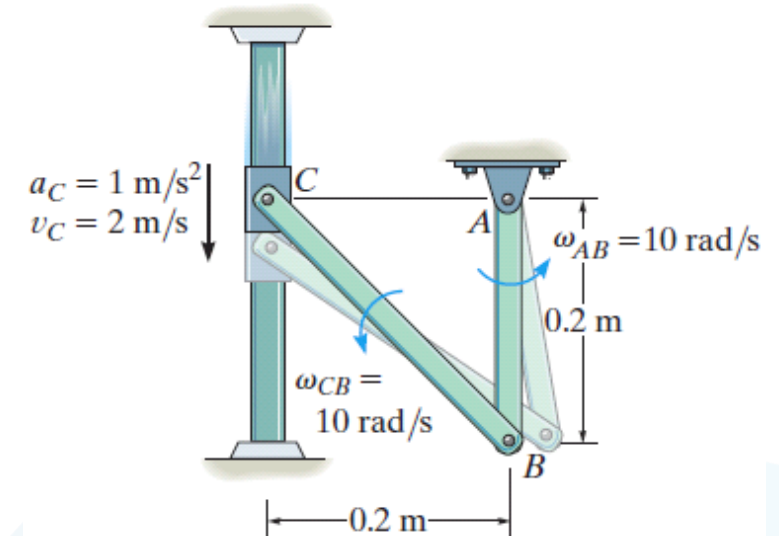
### Acceleration Equation.

Link  $AB$  (rotation about a fixed axis):

$$\mathbf{a}_B = \boldsymbol{\alpha}_{AB} \times \mathbf{r}_B - \omega_{AB}^2 \mathbf{r}_B$$

$$\mathbf{a}_B = (\alpha_{AB} \mathbf{k}) \times (-0.2 \mathbf{j}) - (10)^2 (-0.2 \mathbf{j})$$

$$\mathbf{a}_B = 0.2 \alpha_{AB} \mathbf{i} + 20 \mathbf{j}$$



Note that  $\mathbf{a}_B$  has  $n$  and  $t$  components since it moves along a *circular path*.

Link  $BC$  (general plane motion):

$$\mathbf{a}_B = \mathbf{a}_C + \boldsymbol{\alpha}_{CB} \times \mathbf{r}_{B/C} - \omega_{CB}^2 \mathbf{r}_{B/C}$$

$$0.2\alpha_{AB}\mathbf{i} + 20\mathbf{j} = -1\mathbf{j} + (\alpha_{CB}\mathbf{k}) \times (0.2\mathbf{i} - 0.2\mathbf{j}) - (10)^2(0.2\mathbf{i} - 0.2\mathbf{j})$$

$$0.2\alpha_{AB}\mathbf{i} + 20\mathbf{j} = -1\mathbf{j} + 0.2\alpha_{CB}\mathbf{j} + 0.2\alpha_{CB}\mathbf{i} - 20\mathbf{i} + 20\mathbf{j}$$

Thus,

$$0.2\alpha_{AB} = 0.2\alpha_{CB} - 20$$

$$20 = -1 + 0.2\alpha_{CB} + 20$$

Solving,

$$\alpha_{CB} = 5 \text{ rad/s}^2 \curvearrowright$$

*Ans.*

$$\alpha_{AB} = -95 \text{ rad/s}^2 = 95 \text{ rad/s}^2 \curvearrowright$$

*Ans.*

## EXAMPLE

The crankshaft  $AB$  turns with a clockwise angular acceleration of  $20 \text{ rad/s}^2$ . Determine the acceleration of the piston at the instant  $AB$  is in the position shown. At this instant  $\omega_{AB} = 10 \text{ rad/s}$  and  $\omega_{BC} = 2.43 \text{ rad/s}$ .

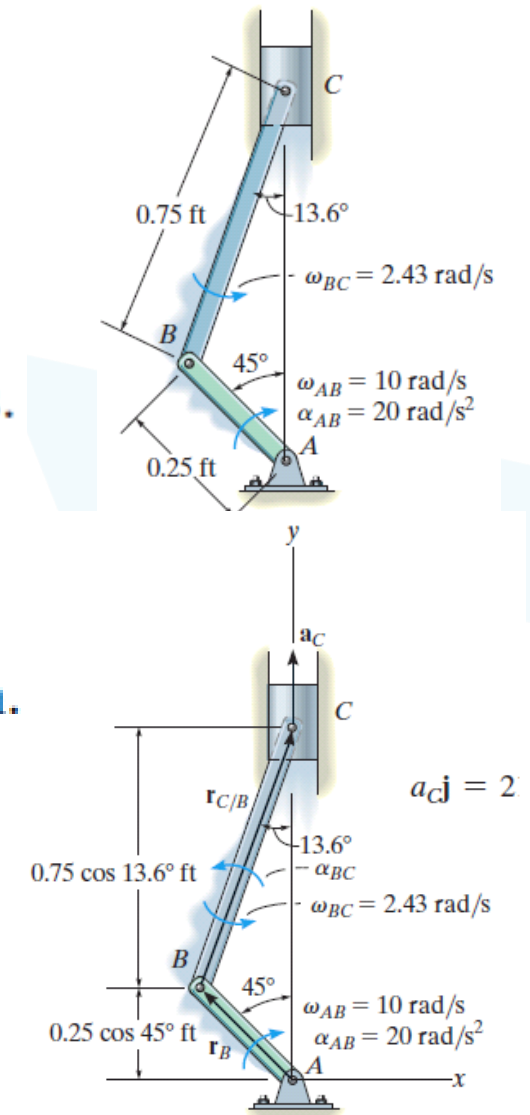
## SOLUTION (VECTOR ANALYSIS)

**Kinematic Diagram.** The kinematic diagrams for both  $AB$  and  $BC$  are shown. Here  $a_C$  is vertical since  $C$  moves along a straight-line path.

**Acceleration Equation.** Expressing each of the position vectors in Cartesian vector form

$$\mathbf{r}_B = \{-0.25 \sin 45^\circ \mathbf{i} + 0.25 \cos 45^\circ \mathbf{j}\} \text{ ft} = \{-0.177 \mathbf{i} + 0.177 \mathbf{j}\} \text{ ft}$$

$$\mathbf{r}_{C/B} = \{0.75 \sin 13.6^\circ \mathbf{i} + 0.75 \cos 13.6^\circ \mathbf{j}\} \text{ ft} = \{0.177 \mathbf{i} + 0.729 \mathbf{j}\} \text{ ft}$$





**Crankshaft  $AB$  (rotation about a fixed axis):**

$$\begin{aligned}
 \mathbf{a}_B &= \boldsymbol{\alpha}_{AB} \times \mathbf{r}_B - \omega_{AB}^2 \mathbf{r}_B \\
 &= (-20\mathbf{k}) \times (-0.177\mathbf{i} + 0.177\mathbf{j}) - (10)^2(-0.177\mathbf{i} + 0.177\mathbf{j}) \\
 &= \{21.21\mathbf{i} - 14.14\mathbf{j}\} \text{ ft/s}^2
 \end{aligned}$$

**Connecting Rod  $BC$  (general plane motion):** Using the result for  $\mathbf{a}_B$  and noting that  $\mathbf{a}_C$  is in the vertical direction, we have

$$\begin{aligned}
 \mathbf{a}_C &= \mathbf{a}_B + \boldsymbol{\alpha}_{BC} \times \mathbf{r}_{C/B} - \omega_{BC}^2 \mathbf{r}_{C/B} \\
 a_C \mathbf{j} &= 21.21\mathbf{i} - 14.14\mathbf{j} + (\alpha_{BC} \mathbf{k}) \times (0.177\mathbf{i} + 0.729\mathbf{j}) - (2.43)^2(0.177\mathbf{i} + 0.729\mathbf{j}) \\
 a_C \mathbf{j} &= 21.21\mathbf{i} - 14.14\mathbf{j} + 0.177\alpha_{BC} \mathbf{j} - 0.729\alpha_{BC} \mathbf{i} - 1.04\mathbf{i} - 4.30\mathbf{j} \\
 0 &= 20.17 - 0.729\alpha_{BC} \\
 a_C &= 0.177\alpha_{BC} - 18.45
 \end{aligned}$$

## Solving yields

$$\alpha_{BC} = 27.7 \text{ rad/s}^2 \curvearrowright$$

$$a_C = -13.5 \text{ ft/s}^2$$

*Ans.*

**NOTE:** Since the piston is moving upward, the negative sign for  $a_C$  indicates that the piston is decelerating, i.e.,  $\mathbf{a}_C = \{-13.5\mathbf{j}\} \text{ ft/s}^2$ . This causes the speed of the piston to decrease until  $AB$  becomes vertical, at which time the piston is momentarily at rest.

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