

An harmonic excitation can be described either by means of a sine function:  $p(t) = p_0 \sin \Omega t$ , or by means of a cosine function:  $p(t) = p_0 \cos \Omega t$ .

**Equation of Motion (E.o.M.):**

معادلة الحركة

$$m\ddot{u} + cu' + ku = p(t) = \begin{cases} p_0 \cos \Omega t \\ p_0 \sin \Omega t \end{cases}$$

حلها هو مجموع حل متجانس (استجابة) (homogenous) and steady-state (particular) components. حل خاص (استجابة دائمة).

$$u(t) = \underbrace{e^{-\xi \omega t} (A \cos \omega_D t + B \sin \omega_D t)}_{\text{transient}} + \underbrace{C \cos \Omega t + D \sin \Omega t}_{\text{steady state}}$$

إيجاد الحل الخاص (استجابة دائمة) Find  $C$  &  $D$ , for the cosine and sine functions of harmonic excitation

## Undamped harmonic vibrations

## الاهتزازات القسرية الهازمونية غير المخمدة

$$m\ddot{u} + ku = p_0 \cos \Omega t \quad \ddot{u} + \omega_n^2 u = \left(\frac{p_0}{m}\right) \cos \Omega t = \left(\frac{p_0}{k}\right) \left(\frac{k}{m}\right) \cos \Omega t \quad \ddot{u} + \omega_n^2 u = \omega_n^2 u_{st} \cos \Omega t$$

يمكن للحل الخاص (استجابة دائمة) أن يأخذ الشكل

$$u_p(t) = C \cos \Omega t \quad \ddot{u}_p(t) = -C \Omega^2 \cos \Omega t \quad (-C \Omega^2 + C \omega_n^2) \cos \Omega t = \omega_n^2 u_{st} \cos \Omega t$$

$$(\omega_n^2 - \Omega^2)C = \omega_n^2 u_{st} \quad C = \frac{\omega_n^2 u_{st}}{(\omega_n^2 - \Omega^2)} \quad C = \frac{u_{st}}{(1 - r^2)} \quad \text{where} \quad r = \frac{\Omega}{\omega_n}$$

The transient response (The homogeneous solution) is

$$u_h(t) = A \cos \omega_n t + B \sin \omega_n t$$

The complete solution is (A homogeneous solution) is

$$u(t) = A \cos \omega_n t + B \sin \omega_n t + \frac{\omega_n^2 u_{st}}{(\omega_n^2 - \Omega^2)} \cos \Omega t$$

## Undamped harmonic vibrations

الاهتزازات القسرية الهازمونية غير المخمدة

$$u(t) = A \cos \omega_n t + B \sin \omega_n t + \frac{\omega_n^2 u_{st}}{(\omega_n^2 - \Omega^2)} \cos \Omega t$$

By means of the initial conditions given by :

$$u(0) = u_0 \quad \& \quad \dot{u}(0) = \dot{u}_0$$

the constants  $A$  and  $B$  can be calculated as follows:

$$A = u_0 - \frac{\omega_n^2 u_{st}}{(\omega_n^2 - \Omega^2)} \quad \& \quad B = \frac{\dot{u}_0}{\omega_n}$$

$$u(t) = \left( u_0 - \frac{\omega_n^2 u_{st}}{(\omega_n^2 - \Omega^2)} \right) \cos \omega_n t + \left( \frac{\dot{u}_0}{\omega_n} \right) \sin \omega_n t + \frac{\omega_n^2 u_{st}}{(\omega_n^2 - \Omega^2)} \cos \Omega t$$

For two null initial conditions the complete solution is,

$$u(0) = 0 \quad \& \quad \dot{u}(0) = 0$$

$$u(t) = \frac{\omega_n^2 u_{st}}{(\omega_n^2 - \Omega^2)} (\cos \Omega t - \cos \omega_n t)$$

## Undamped harmonic vibrations

الاهتزازات القسرية الهازمونية غير المخمدة

$$u(t) = \frac{\omega_n^2 u_{st}}{(\omega_n^2 - \Omega^2)} (\cos \Omega t - \cos \omega_n t)$$

Using the trigonometric identity

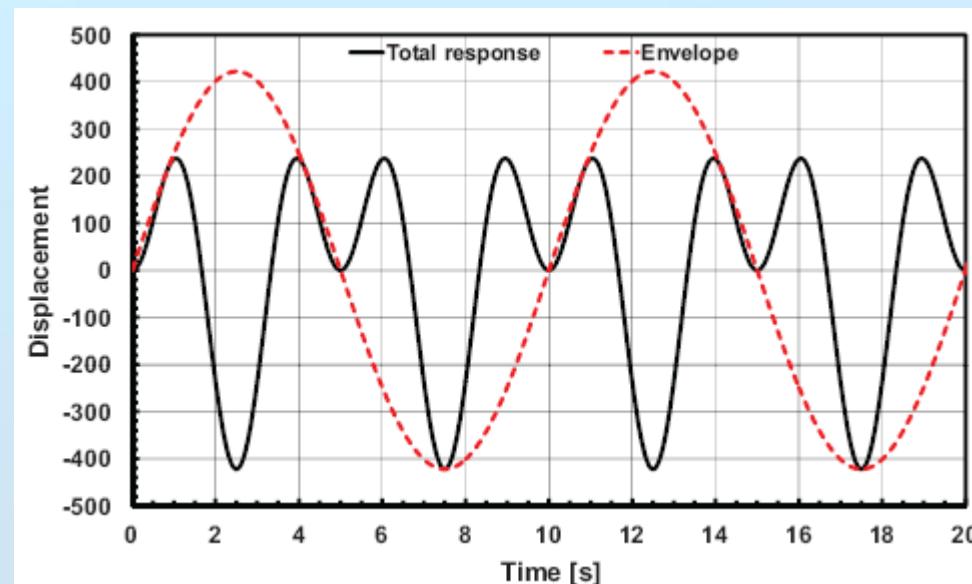
$$\cos \alpha - \cos \beta = -2 \sin \frac{\alpha - \beta}{2} \sin \frac{\alpha + \beta}{2}$$

We get

$$u(t) = \frac{2\omega_n^2 u_{st}}{(\Omega^2 - \omega_n^2)} \sin\left(\frac{\Omega - \omega_n}{2}t\right) \sin\left(\frac{\Omega + \omega_n}{2}t\right)$$

Case 1: Natural frequency SDoF 0.2 Hz, excitation frequency 0.4 Hz.  $\Omega / \omega_n = 2$

$$u(t) = \frac{2u_{st}}{3} \sin(0.2\pi t) \sin(0.6\pi t)$$



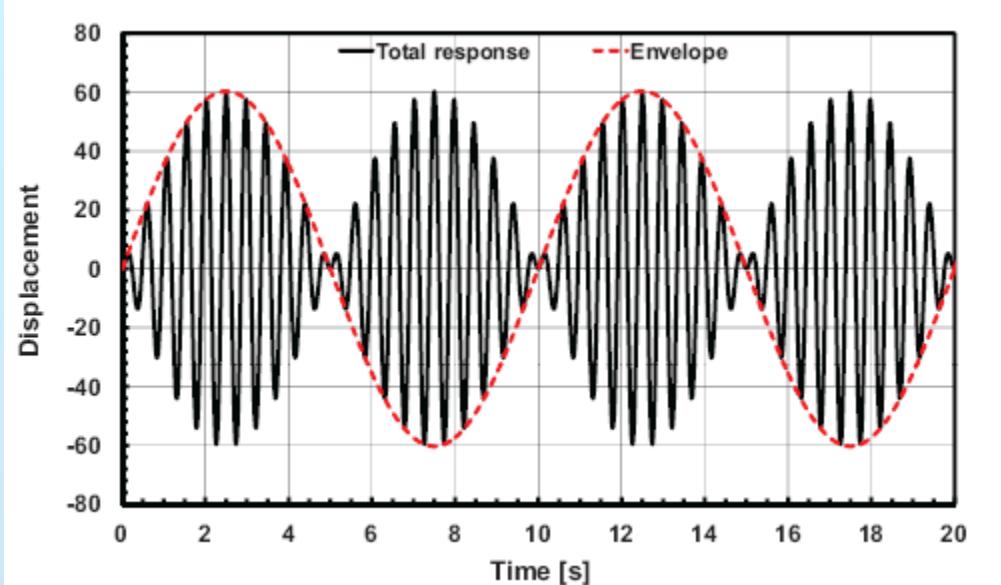
## Undamped harmonic vibrations

## الاهتزازات القسرية الهازمونية غير المخمدة

$$u(t) = \frac{2\omega_n^2 u_{st}}{(\Omega^2 - \omega_n^2)} \sin\left(\frac{\Omega - \omega_n}{2}t\right) \sin\left(\frac{\Omega + \omega_n}{2}t\right)$$

Case 2: Natural frequency SDoF 2.0 Hz, excitation frequency 2.2 Hz.  $\Omega / \omega_n = 1.1$

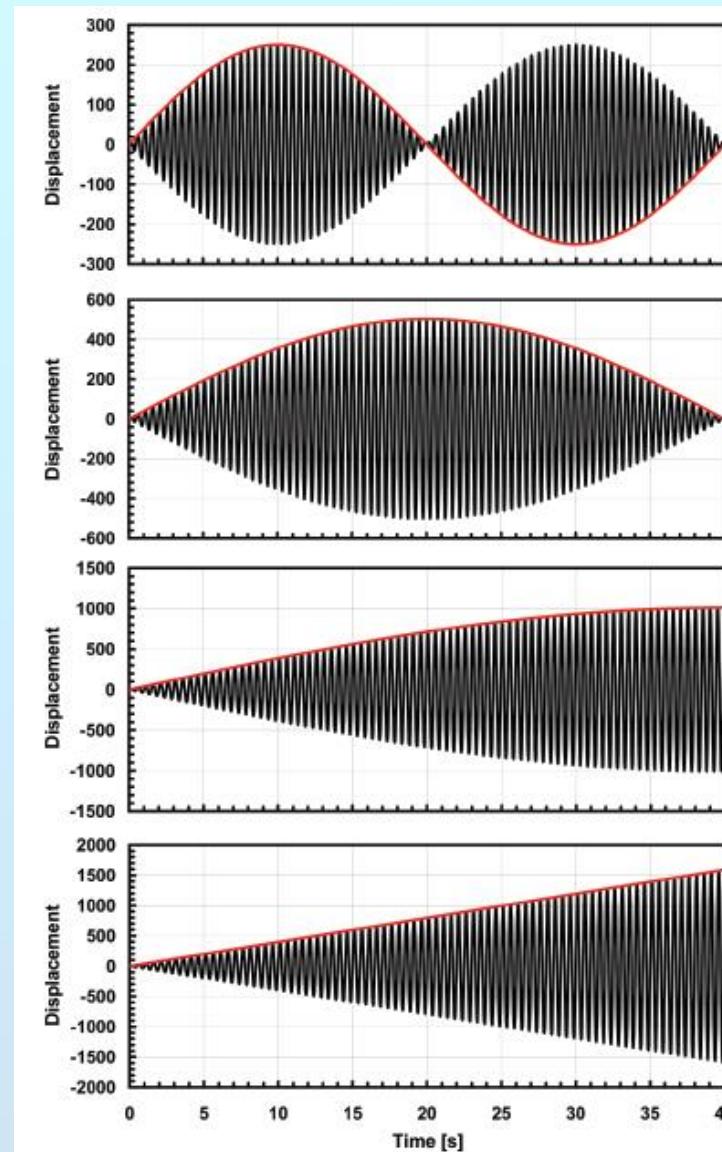
$$u(t) = 9.52u_{st} \sin(0.2\pi t) \sin(4.2\pi t)$$



A beat is always present, but is more evident when the natural frequency of the SDoF system and the excitation frequency are close

# الاستجابة للتحريض الهازموني (المثلثي) الاهتزازات القسرية الهازمونية غير المخمدة

## Response to Harmonic Excitation Undamped harmonic vibrations



$$\Omega / \omega_n = 1.025$$

$$\Omega / \omega_n = 1.0125$$

$$\Omega / \omega_n = 1.00625$$

$$\Omega / \omega_n = 1. \text{ Resonance}$$

## Undamped harmonic vibrations

## الاهتزازات القسرية الهازمونية غير المخمدة

### Resonant excitation ( $\Omega = \omega_n$ )

$$\ddot{u} + \omega_n^2 u = \omega_n^2 u_{st} \cos \Omega t$$

$$\ddot{u} + \omega_n^2 u = \omega_n^2 u_{st} \cos \omega_n t$$

A steady-state response (A particular solution) could not be  $u_p(t) = C \cos \omega_n t$

Another possible choice is  $u_p(t) = C t \sin \omega_n t$

$$\dot{u}_p(t) = C \sin \omega_n t + C t \omega_n \cos \omega_n t$$

$$\ddot{u}_p(t) = 2C \omega_n \cos \omega_n t - C t \omega_n^2 \sin \omega_n t$$

Substituting into the E. o. M.

$$2C \omega_n \cos \omega_n t - C t \omega_n^2 \sin \omega_n t + C t \omega_n^2 \sin \omega_n t = \omega_n^2 u_{st} \cos \omega_n t \quad 2C = \omega_n u_{st}$$

So the particular solution is

$$u_p(t) = \left( \frac{\omega_n u_{st}}{2} \right) t \sin \omega_n t$$

## Undamped harmonic vibrations

## الاهتزازات القسرية الهازمونية غير المخمدة

The transient response (The homogeneous solution) is

$$u_h(t) = A \cos \omega_n t + B \sin \omega_n t$$

The complete solution is (A homogeneous solution) is

$$u(t) = A \cos \omega_n t + B \sin \omega_n t + \left( \frac{\omega_n u_{st}}{2} \right) t \sin \omega_n t$$

By means of the initial conditions given by ,  $u(0) = u_0$  &  $\dot{u}(0) = \dot{u}_0$

the constants  $A$  and  $B$  can be calculated as follows:  $A = u_0$  &  $B = \dot{u}_0 / \omega_n$

$$u(t) = u_0 \cos \omega_n t + \left( \frac{\dot{u}_0}{\omega_n} \right) \sin \omega_n t + \left( \frac{\omega_n u_{st}}{2} \right) t \sin \omega_n t$$

For two null initial conditions the homogeneous part of the solution falls away and the complete solution reduces to the particular solution,

$$u(t) = \left( \frac{\omega_n u_{st}}{2} \right) t \sin \omega_n t$$

## Undamped harmonic vibrations

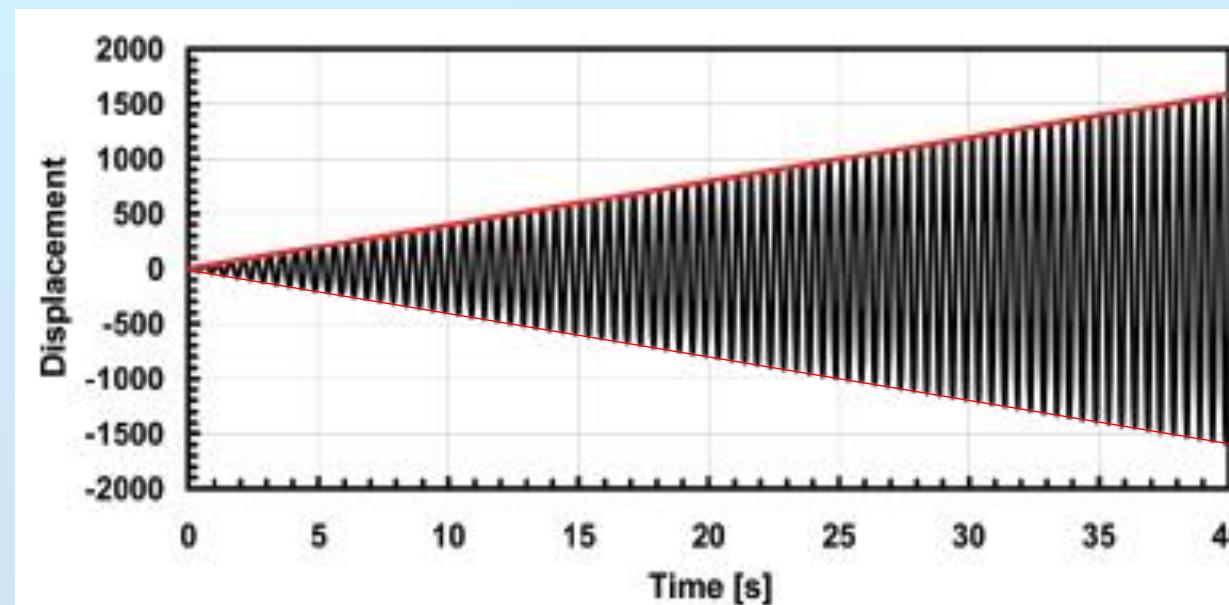
الاهتزازات القسرية الهازمونية غير المخمدة

$$u(t) = \left( \frac{\omega_n u_{st}}{2} \right) t \sin \omega_n t$$

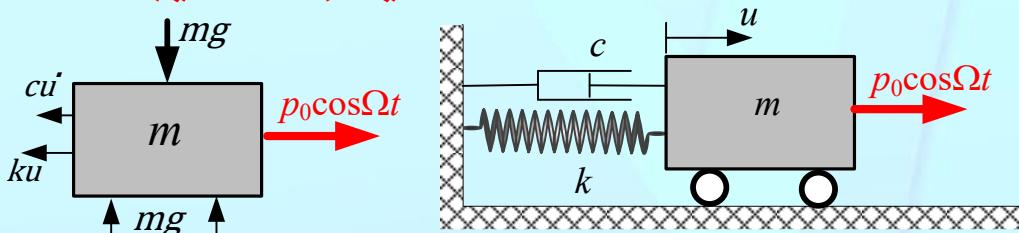
This is a sinusoidal vibration with increasing amplitude:  $C = (\omega_n u_{st}/2)t$ .

The amplitude grows linearly with time and when:  $t \rightarrow \infty$ ,  $C \rightarrow \infty$ .

After infinite time the amplitude of the vibration is infinite as well.



## Damped harmonic vibrations



$$m\ddot{u} + cu + ku = p_0 \cos \Omega t$$

$$\ddot{u} + 2\xi\omega_n\dot{u} + \omega_n^2 u = (p_0 / m) \cos \Omega t$$

Canonical E. o. M.  $\ddot{u} + 2\xi\omega_n\dot{u} + \omega_n^2 u = \omega_n^2 u_{st} \cos \Omega t$

Particular solution

$$u_p(t) = C \cos \Omega t + D \sin \Omega t$$

$$\dot{u}_p(t) = -C\Omega \sin \Omega t + D\Omega \cos \Omega t$$

$$\ddot{u}_p(t) = -C\Omega^2 \cos \Omega t - D\Omega^2 \sin \Omega t \quad \text{Sub. Into E. o. M.}$$

$$-C\Omega^2 \cos \Omega t - D\Omega^2 \sin \Omega t + 2\xi\omega_n(-C\Omega \sin \Omega t + D\Omega \cos \Omega t) + \omega_n^2 u = \omega_n^2 u_{st} \cos \Omega t$$

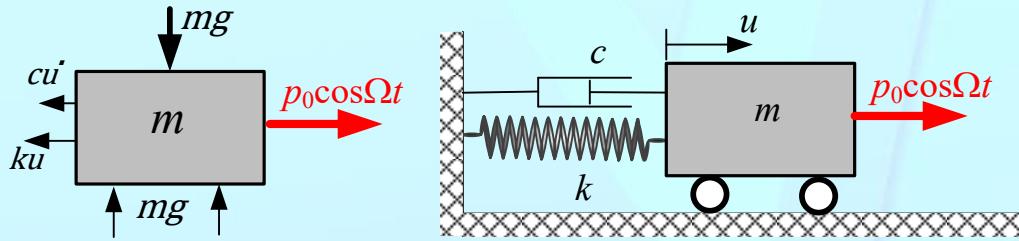
$$((\omega_n^2 - \Omega^2)C + 2\xi\omega_n\Omega D) \cos \Omega t + (-2\xi\omega_n\Omega C + (\omega_n^2 - \Omega^2)D) \sin \Omega t = \omega_n^2 u_{st} \cos \Omega t$$

This is true at any time  $t$ , So

$$\left. \begin{aligned} (\omega_n^2 - \Omega^2)C + 2\xi\omega_n\Omega D &= \omega_n^2 u_{st} \\ -2\xi\omega_n\Omega C + (\omega_n^2 - \Omega^2)D &= 0 \end{aligned} \right\} \Rightarrow \left\{ \begin{aligned} C &= \omega_n^2 u_{st} \frac{(\omega_n^2 - \Omega^2)}{(\omega_n^2 - \Omega^2)^2 + (2\xi\omega_n\Omega)^2} \\ D &= \omega_n^2 u_{st} \frac{2\xi\omega_n\Omega}{(\omega_n^2 - \Omega^2)^2 + (2\xi\omega_n\Omega)^2} \end{aligned} \right.$$

# Response to Harmonic Excitation

## Damped harmonic vibrations



**Canonical E. o. M.**  $\ddot{u} + 2\xi\omega_n\dot{u} + \omega_n^2 u = \omega_n^2 u_{st} \cos \Omega t$

**Particular solution**  $u_p(t) = C \cos \Omega t + D \sin \Omega t$

$$C = \omega_n^2 u_{st} \frac{(\omega_n^2 - \Omega^2)}{(\omega_n^2 - \Omega^2)^2 + (2\xi\omega_n\Omega)^2} \quad \text{and} \quad D = \omega_n^2 u_{st} \frac{2\xi\omega_n\Omega}{(\omega_n^2 - \Omega^2)^2 + (2\xi\omega_n\Omega)^2}$$

$$u_h(t) = e^{-\xi\omega_n t} (A \cos \omega_D t + B \sin \omega_D t) \quad \text{with} \quad \omega_D = \omega_n \sqrt{1 - \xi^2}$$

By means of the initial conditions the constants  $A$  and  $B$ , can be determined

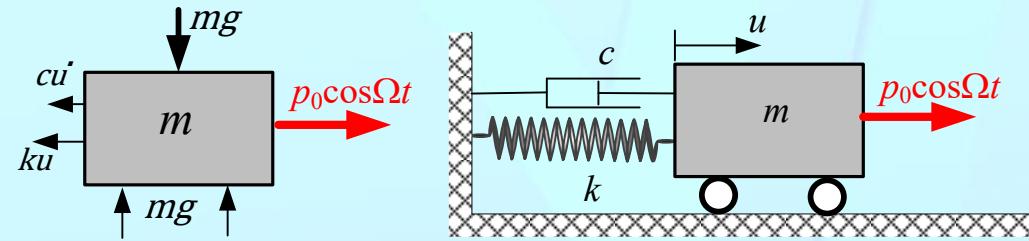
Denominations:

- Homogeneous part of the solution: “**transient**”
- Particular part of the solution: “**steady-state**”

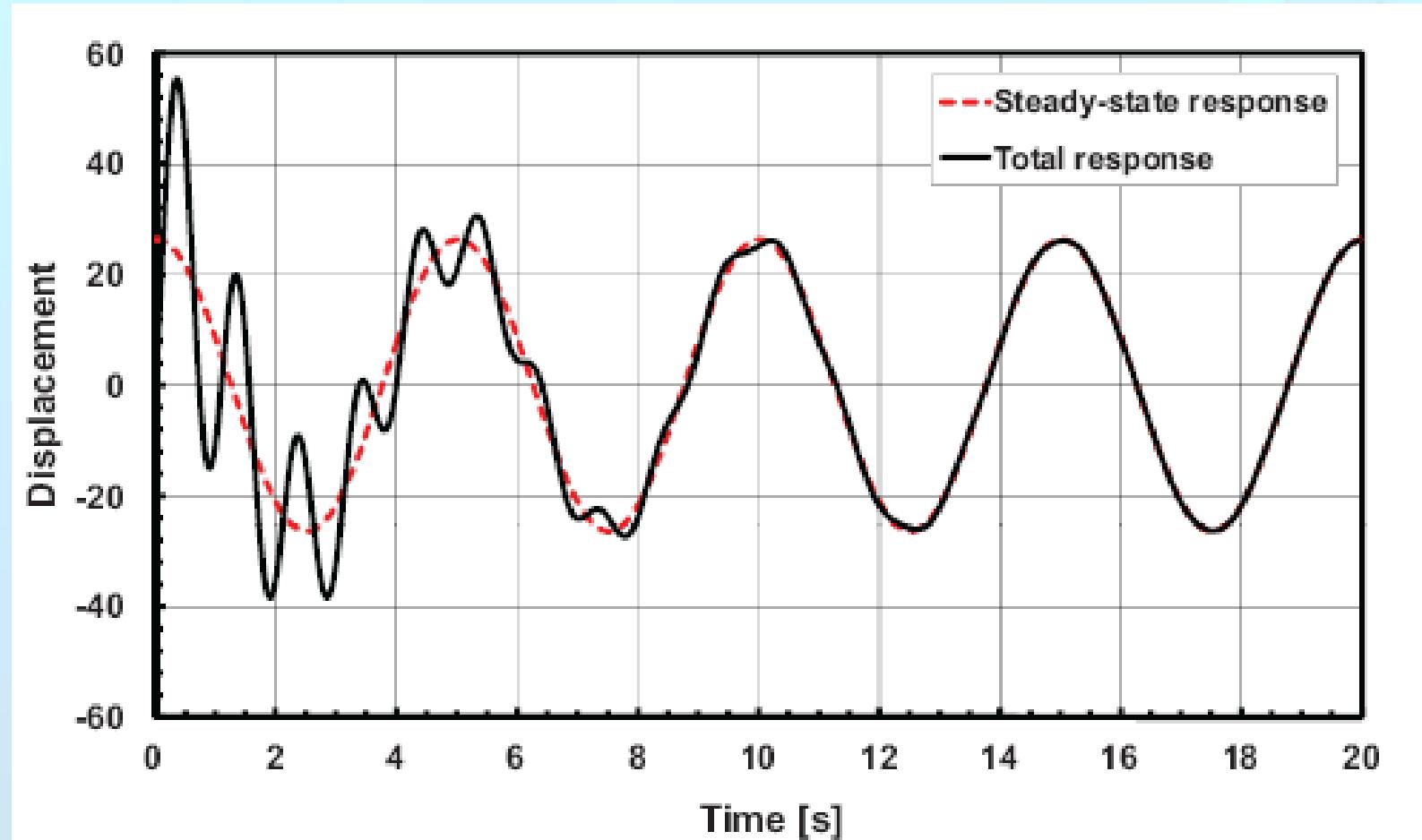
Visualization of the solution is illustrated in the next example

# Response to Harmonic Excitation

## Damped harmonic vibrations



Example 1:  $\omega_n = 2\pi$  [rad/sec],  $\Omega = 0.4\pi$  [rad/sec],  $\xi = 5\%$ ,  $u_{st} = 25\text{mm}$ ,  $u_0 = 0$ ,  $\dot{u}_0 = u_{st}\omega_n$



# Response to Harmonic Excitation

**Damped harmonic vibrations**

**Resonant excitation ( $\Omega = \omega_n$ )**

**Canonical E. o. M.**  $\ddot{u} + 2\xi\omega_n\dot{u} + \omega_n^2 u = \omega_n^2 u_{st} \cos \Omega t$

$$u_p(t) = C \cos \Omega t + D \sin \Omega t$$

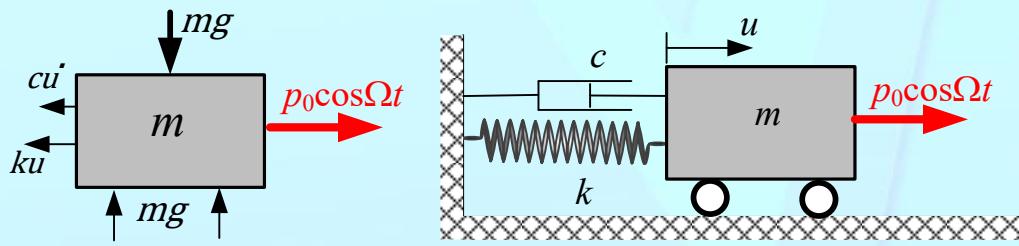
$$C = \omega_n^2 u_{st} \frac{(\omega_n^2 - \Omega^2)}{(\omega_n^2 - \Omega^2)^2 + (2\xi\omega_n\Omega)^2} \quad \text{and} \quad D = \omega_n^2 u_{st} \frac{2\xi\omega_n\Omega}{(\omega_n^2 - \Omega^2)^2 + (2\xi\omega_n\Omega)^2}$$

By substituting ( $\Omega = \omega_n$ ) in the two expressions constants  $C$  and  $D$ , becomes:

$$C = 0 \quad \text{and} \quad D = \frac{u_{st}}{2\xi}$$

This means that if damping is present, the resonant excitation is not a special case anymore, and the complete solution of the differential equation is:

$$u(t) = e^{-\xi\omega_n t} (A \cos \omega_D t + B \sin \omega_D t) + \frac{u_{st}}{2\xi} \sin \omega_n t$$



# Response to Harmonic Excitation

Damped harmonic vibrations

Resonant excitation ( $\Omega = \omega_n$ )

Canonical E. o. M.  $\ddot{u} + 2\xi\omega_n\dot{u} + \omega_n^2 u = \omega_n^2 u_{st} \cos \Omega t$

$$u_p(t) = C \cos \Omega t + D \sin \Omega t$$

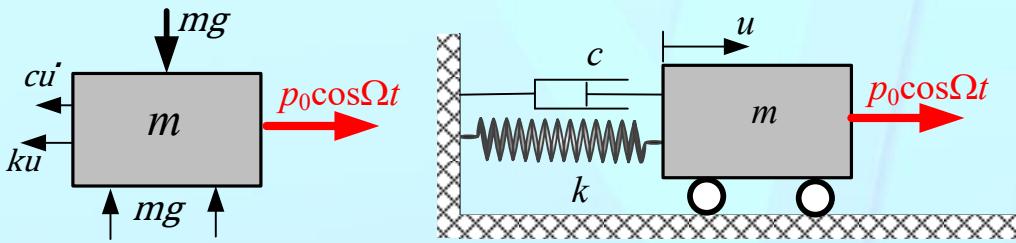
$$C = \omega_n^2 u_{st} \frac{(\omega_n^2 - \Omega^2)}{(\omega_n^2 - \Omega^2)^2 + (2\xi\omega_n\Omega)^2} \quad \text{and} \quad D = \omega_n^2 u_{st} \frac{2\xi\omega_n\Omega}{(\omega_n^2 - \Omega^2)^2 + (2\xi\omega_n\Omega)^2}$$

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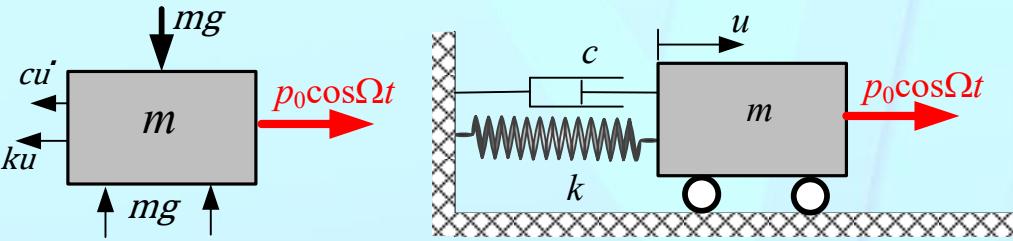
$$u(t) = e^{-\xi\omega_n t} (A \cos \omega_D t + B \sin \omega_D t) + \frac{u_{st}}{2\xi} \sin \omega_n t$$



# Response to Harmonic Excitation

## Damped harmonic vibrations

### Resonant excitation ( $\Omega = \omega_n$ )



$$u(t) = e^{-\xi\omega_n t} (A \cos \omega_D t + B \sin \omega_D t) + \frac{u_{st}}{2\xi} \sin \omega_n t$$

By means of the initial conditions the constants  $A$  and  $B$ , can be determined.  
For example in the special case,  $u_0 = 0$  &  $\dot{u}_0 = 0$ ,  $A$  &  $B$ , are

$$A = 0 \quad \text{and} \quad B = -\frac{u_{st}}{2\xi\sqrt{1-\xi^2}}$$

$$u(t) = \frac{u_{st}}{2\xi} \left( \sin \omega_n t - \frac{e^{-\xi\omega_n t}}{\sqrt{1-\xi^2}} \sin \omega_D t \right)$$

After a certain time, the **homogeneous part** of the solution vanishes and what remains is a sinusoidal oscillation of the maximum limited amplitude: ( $u_{\max} = u_{st}/2\xi$ )

For small damping ratios ( $\xi < 0.2$ ),  $\omega_n \approx \omega_D$  and  $(1 - \xi)^{1/2} \approx 1$ , hence  $u(t)$  becomes:

$$u(t) = u_{\max} \left( 1 - e^{-\xi\omega_n t} \right) \sin \omega_n t$$

# Response to Harmonic Excitation

## Damped harmonic vibrations

### Dynamic Amplification Factor

The steady-state displacement of a system due to harmonic excitation is the dominant part of its response. This steady-state response is given by

$$u_p(t) = C \cos \Omega t + D \sin \Omega t$$

Where  $C = \omega_n^2 u_{st} \frac{(\omega_n^2 - \Omega^2)}{(\omega_n^2 - \Omega^2)^2 + (2\xi\omega_n\Omega)^2}$  and  $D = \omega_n^2 u_{st} \frac{2\xi\omega_n\Omega}{(\omega_n^2 - \Omega^2)^2 + (2\xi\omega_n\Omega)^2}$

By means of the trigonometric identity:

$$a \cos \alpha + b \sin \alpha = (a^2 + b^2)^{1/2} \cos(\alpha - \beta) \quad \text{with} \quad \tan \beta = b/a$$

The steady-state response can be transformed as follows

$$u_p(t) = u_{\max} \cos(\Omega t - \varphi)$$

It is a cosine vibration with the maximum dynamic amplitude  $u_{\max}$ , given by

$$u_{\max} = (C^2 + D^2)^{1/2}$$

and the phase angle  $\varphi$  obtained from:

$$\tan \varphi = D / C$$

# Response to Harmonic Excitation

## Damped harmonic vibrations

Dynamic Amplification Factor

Substitution of  $C$  and  $D$ , in  $u_{\max}$  expression gives

$$u_{\max} = \sqrt{\left[ \omega_n^2 u_{st} \frac{(\omega_n^2 - \Omega^2)}{(\omega_n^2 - \Omega^2)^2 + (2\xi\omega_n\Omega)^2} \right]^2 + \left[ \omega_n^2 u_{st} \frac{2\xi\omega_n\Omega}{(\omega_n^2 - \Omega^2)^2 + (2\xi\omega_n\Omega)^2} \right]^2}$$

$$u_{\max} = \omega_n^2 u_{st} \sqrt{\left[ \frac{(\omega_n^2 - \Omega^2)}{(\omega_n^2 - \Omega^2)^2 + (2\xi\omega_n\Omega)^2} \right]^2 + \left[ \frac{2\xi\omega_n\Omega}{(\omega_n^2 - \Omega^2)^2 + (2\xi\omega_n\Omega)^2} \right]^2}$$

$$u_{\max} = \omega_n^2 u_{st} \sqrt{\frac{(\omega_n^2 - \Omega^2)^2 + (2\xi\omega_n\Omega)^2}{\left[ (\omega_n^2 - \Omega^2)^2 + (2\xi\omega_n\Omega)^2 \right]^2}}$$

$$u_{\max} = \omega_n^2 u_{st} \frac{1}{\sqrt{(\omega_n^2 - \Omega^2)^2 + (2\xi\omega_n\Omega)^2}}$$

$$u_{\max} = u_{st} \frac{1}{\sqrt{\left(1 - (\Omega/\omega_n)^2\right)^2 + (2\xi(\Omega/\omega_n))^2}} \quad \text{DAF} = \frac{u_{\max}}{u_{st}} = \frac{1}{\sqrt{\left(1 - (\Omega/\omega_n)^2\right)^2 + (2\xi(\Omega/\omega_n))^2}}$$

# Response to Harmonic Excitation

## Damped harmonic vibrations

### Dynamic Amplification Factor

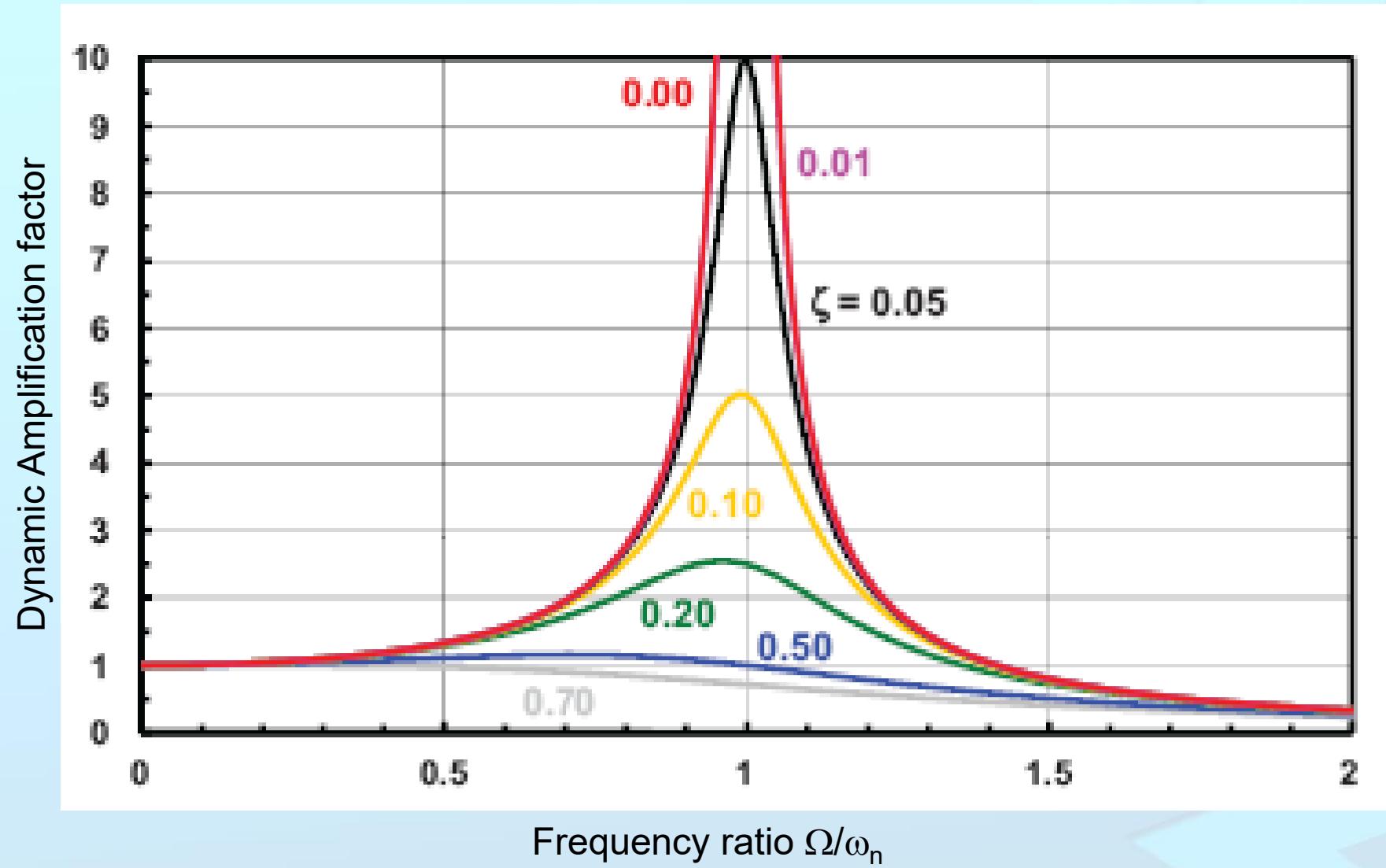
Substitution of  $C$  and  $D$ , in  $\tan\varphi$  expression gives

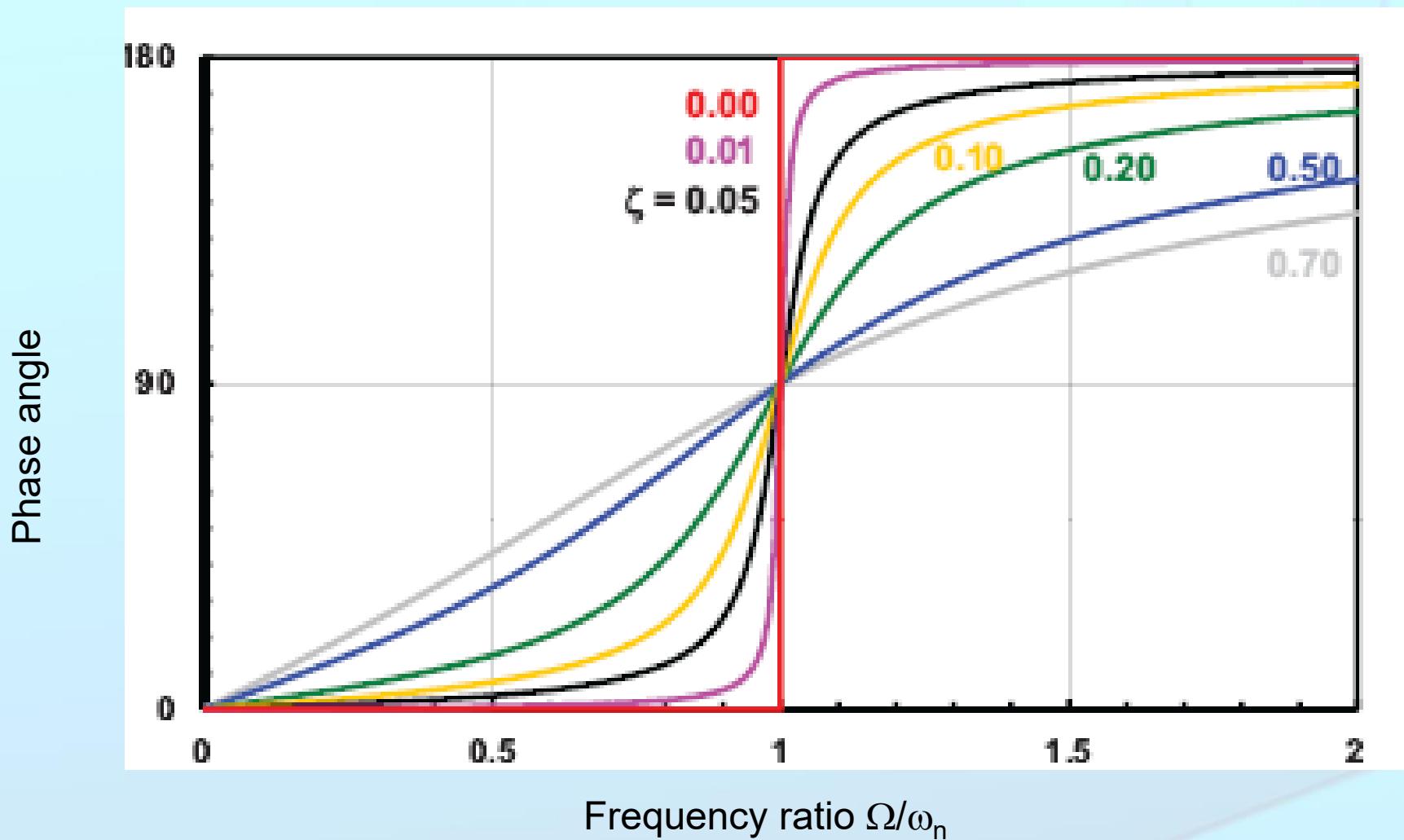
$$\tan\varphi = \frac{D}{C} = \frac{2\xi\omega_n\Omega}{(\omega_n^2 - \Omega^2)} = \frac{2\xi(\Omega/\omega_n)}{1 - (\Omega/\omega_n)^2}$$

Defining the ratio  $r = \Omega/\omega_n$ , the two expressions simplify to

$$\text{DAF} = \frac{u_{\text{max}}}{u_{\text{st}}} = \frac{1}{\sqrt{(1-r^2)^2 + (2\xi r)^2}}$$

$$\tan\varphi = \frac{2\xi r}{1-r^2}$$





Ex. 1. An undamped oscillator is driven by an harmonic loading. If the static displacement is  $u_{st} = 0.05\text{m}$ , determine the displacement response amplitude for the following frequency ratios:  $r = 0.2, 0.9, 1.1, 1.8 \text{ & } 3.0$ .

Ex. 2 An undamped system consisting of a 10 kg mass and a spring of stiffness  $k = 4 \text{ kN/m}$  is acted upon by a harmonic force of magnitude  $P_0 = 0.5 \text{ kN}$ . The displacement amplitude of the steady-state response was observed to be 11 cm. Determine the frequency of the excitation force.

Ex. 3. An undamped system having a mass of 50 kg is excited by a harmonic force with magnitude  $P_0=100$  N and an operating frequency of 10 Hz. The displacement amplitude of the steady-state response was observed to be 3.2 mm. Determine the spring constant  $k$  of the system.

Ex. 4. An undamped system having a mass of 10 kg and a spring of constant of  $k = 8$  N/mm is excited by a harmonic force with magnitude  $F_0 = 200$  N and an operating frequency of 35 rad/sec. If the initial displacement is 21 mm and the initial velocity is 175 mm/sec, determine the total displacement, velocity and acceleration of the mass at (a)  $t = 2$  sec, (b)  $t = 4$  sec and (c)  $t = 6$  sec.

$$u(t) = \left( u_0 - \frac{\omega_n^2 u_{st}}{(\omega_n^2 - \Omega^2)} \right) \cos \omega_n t + \left( \frac{\dot{u}_0}{\omega_n} \right) \sin \omega_n t + \frac{\omega_n^2 u_{st}}{(\omega_n^2 - \Omega^2)} \cos \Omega t$$

Ex.5. An undamped spring-mass system having a mass of 4.5 kg and a spring of constant of  $k = 3.5$  N/mm is excited by a harmonic force with magnitude  $F_0 = 100$  N and an operating frequency of 18 rad/sec. If the initial displacement is 15 mm and the initial velocity is 150 mm/sec, determine

- (a) The frequency ratio
- (b) The amplitude of the forced response
- (c) The displacement of the mass at  $t = 2$  sec

Ex. 6. A portable eccentric mass shaker is sometimes used to evaluate the *in situ* dynamic properties of a structure, using two different frequencies and measuring the displacement amplitudes as well as the phase angles. Such a test was carried out on a single story building and the following responses were recorded:

- (1) at  $\Omega_1=18.30$  rad/s,  $P_{01}=837$  kN,  $u_{\max 1}= 1.39$ mm &  $\varphi_1=8^\circ$ ;
- (2) at  $\Omega_2=60.99$  rad/s,  $P_{02}= 9300$  kN,  $u_{\max 2}= 3.32$ mm &  $\varphi_2=174.29^\circ$ .

Compute the natural frequency  $\omega_n$  & the damping ratio  $\xi$  for the structure

$$\text{DAF} = \frac{u_{\max}}{u_{st}} = \frac{1}{\sqrt{(1-r^2)^2 + (2\xi r)^2}} \quad \tan \varphi = \frac{2\xi r}{1-r^2}$$

$$u_{\max} = \frac{u_{st}}{(1-r^2)} \frac{1}{\sqrt{1 + [(2\xi r)/(1-r^2)]^2}} = \frac{u_{st} \cos \varphi}{(1-r^2)}$$

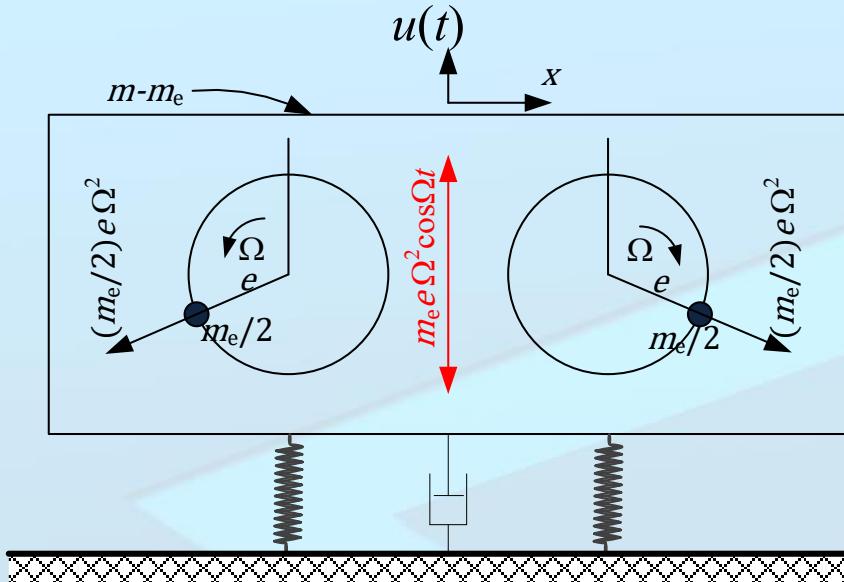
$$u_{\max} = \frac{u_{st} \cos \varphi}{(1-r^2)} = \frac{u_{st} \omega_n^2 \cos \varphi}{(\omega_n^2 - \Omega^2)} = \frac{P_0 \omega_n^2 \cos \varphi}{k(\omega_n^2 - \Omega^2)} = \frac{P_0 \cos \varphi}{m(\omega_n^2 - \Omega^2)}$$

$$\frac{\omega_n^2 - \Omega_2^2}{\omega_n^2 - \Omega_1^2} = \frac{(u_{\max})_1 P_{02} \cos \varphi_2}{(u_{\max})_2 P_{01} \cos \varphi_1} = \frac{1.39 \times 9300 \times \cos 174.29^\circ}{3.32 \times 837 \times \cos 8^\circ} = -4.67435$$

$$\omega_n^2 = \frac{\Omega_2^2 + 4.67435\Omega_1^2}{5.67435} \Rightarrow \omega_n = 30.5 \text{ rad/s}$$

$$\xi = \frac{(1-r_{1,2}^2) \tan \varphi_{1,2}}{2r_{1,2}} = \frac{[1 - (\Omega_1/\omega_n)^2] \tan \varphi_1}{2(\Omega_1/\omega_n)} = \frac{[1 - (18.3/30.5)^2] \tan 8^\circ}{2(18.3/30.5)} = 0.075$$

$$\frac{1}{\sqrt{1 + [(2\xi r)/(1-r^2)]^2}} = \frac{1}{\sqrt{1 + \tan^2 \varphi}} = \cos \varphi$$



Ex.7. A Structure having a mass of 100 kg and a translational stiffness of 40000 N/m is excited by a harmonic force with magnitude  $F_0=500$  N and an operating frequency of 2.5 Hz. The damping ratio for the structure is 0.10. For the steady-state vibration determine

- (a) The amplitude of the steady-state displacement
- (b) Its phase with respect to the exciting force, and
- (c) The maximum velocity of the response